# Proposed East Milford Mixed Use Development Nova Scotia Department of Public Works 

Traffic Impact Study<br>Final Report

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## RE: Traffic Impact Study for a proposed residential development in East Milford

The GRIFFIN transportation group inc. is pleased to present the results of the enclosed traffic impact study carried out in support of the planning approval process for a proposed Mixed Use neighbourhood in East Milford, Municipality of East Hants (MEH). The proposed development is being planned to contain up to 1,551 residential units and up to $47,000 \mathrm{ft}^{2}$ of supporting commercial space. The entire development will be situated on the PID \#45089802 lands, which measure about 275 acres in size.

A comprehensive traffic operational assessment has been carried out to understand the future impacts of a full build-out scenario of the proposed development. Our analysis also considered additional traffic associated with a number of other adjacent future neighbourhoods in the Lantz area. The results flowing from our analysis suggest that the traffic generated by the proposed development can be accommodated on the study area road network with the enclosed study recommendations in place.

The opening of the new Lantz interchange and Lantz Connector Road has introduced planning approval opportunities for several large-scale residential neighbourhoods in the Lantz area. The magnitude of these developments has exceeded previous long-term municipal servicing and transportation estimates for this area. Although the full build-out of this area is expected to occur over a long period of time (i.e. beyond 30-40 years), it is recommended that the NSDPW begin the planning process to preserve right-of-way for another Highway 102 interchange to serve the transportation needs for this growing area.

It has been a pleasure working with the project team in completing this study. Feel free to contact the undersigned anytime to further discuss the details of this project.


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## 1. INTRODUCTION

### 1.1 Background

The GRIFFIN transportation group inc. (GRIFFIN) has been retained by FH Development Group Ltd. (FH Development) to carry out a traffic impact study assessment for a proposed Mixed Use neighbourhood near the community boundary between Lantz and East Milford, Municipality of East Hants (MEH). The proposed development will occur on undeveloped lands contained within in PID \#45089802 and are generally located between the Highway 102 and Trunk Highway 2 corridors, as shown in Figure 1.

FH Development, the proponent, has plans to develop the subject lands into a Mixed Use neighbourhood that will be comprised of up to 1,551 residential units, and about $47,000 \mathrm{ft}^{2}$ of supporting commercial floor space. The density of the proposed development is expected to be approximately 5.6 units/acre. There are plans to construct the development in phases; however, our analysis has only evaluated the impacts of a full build scenario.

### 1.2 Context

It is understood that the proponent has been working with the Municipality of East Hants (MEH) to meet the necessary planning approval requirements associated with the development of these lands. One of the key requirements is to obtain approval for all new street and access connections that can accommodate vehicle movements in/out of the new development. Since the surrounding public roadways are under the jurisdiction of the Nova Scotia Department of Public Works (NSDPW), it was therefore, necessary to engage with them separately as the approving road agency for this particular study.

To initiate this process, GRIFFIN attended a scope development meeting with representatives of NSDPW on Wednesday November $9^{\text {th }}, 2022$. The discussions followed NSDPW guidelines to identify the general assumptions, intersections to be evaluated, and other relevant details to consider in the traffic assessment process. These steps are detailed in NSDPW's Policy Number P01018 which includes the Traffic Impact Analysis Pre-Study Meeting Checklist. A detailed discussion of each item in the checklist was documented in GRIFFIN's March $6^{\text {th }}, 2023$ traffic impact study scoping document. The final scoping document was submitted to NSDPW for review and approval.

The terms of reference for this impact study were developed based on the following:

- A scope development meeting held on Wednesday November $9^{\text {th }}, 2023$ and attended by representatives of NSDPW, GRIFFIN (sub-consultant), and the proponent.
- The NSDPW-approved TIS Scoping Document prepared by GRIFFIN, dated March $6{ }^{\text {th }}$, 2023.
- The latest version of NSDPW's traffic impact study guidelines document.
- A site plan concept sketch provided by the proponent.
- Multiple site reviews and traffic volume counts carried out by GRIFFIN during November 2022.
- Historical traffic data gathered by NSDPW in the vicinity of the proposed development.

The approach and technical findings of this traffic impact study are discussed in the following sections of this report.

Figure 1: Key Map and Site Location


Source: MEH GIS Map

## 2. EXISTING CONDITIONS

This chapter describes the roadway network, traffic volumes, operating conditions, and other notable characteristics under the baseline conditions.

### 2.1 The Study Area Road Network

The proposed development is generally located west of Trunk 2, north of Robert Scott Drive, and east of Highway 102. The Trunk 2 corridor will be the focus of this study as it will provide the only vehicle access for future residents and patrons. This is an important north-south route that links the communities of Lantz and Elmsdale - to the south - with the communities of Milford and Shubenacadie - to the north.

Regional travel is facilitated via the Highway 102 corridor. Access to this north-south controlledaccess highway is provided via the recently opened Lantz Connector Road - located about 3 km to the south of the proposed development.

Based on the layout and configuration of the existing road network, and through our discussions with NSDPW, it was agreed the traffic impact assessment would focus on the Trunk 2 and Lantz Connector Road corridors.

### 2.2 Existing Traffic Data and Peak Traffic Volumes

Following industry best practices, specific hours that experience the highest traffic volumes on the roadway are applied to the analysis steps in the traffic impact study process to identify the capacity needs required to accommodate peak vehicle demands. Ideally the peak hours for this analysis would occur during the peak travel times along the Trunk 2 and Lantz Connector Road corridors combined with the peak travel time for the proposed Mixed Use development. Historical traffic volume trends from the study area suggest there is a notable peak in weekday commuter flows (i.e. the morning and afternoon travel peaks). This, combined with an expected increase in residential travel associated with the proposed development suggests that the weekday morning and afternoon travel peaks are appropriate for use in this analysis.

To facilitate an assessment of the existing and future traffic operations there was a need to first develop a set of baseline traffic volumes. Although the NSDPW has some recorded historical traffic volume data, GRIFFIN gathered supplementary traffic volume data to provide a more current understanding of the travel demand and travel patterns in the study area. Current peak period traffic volume data collection locations are summarized in Table 1.

Table 1: Current Traffic Data Collection By Location

| Location of Data Collection | AM Peak Period <br> Counts $^{\mathbf{A}}$ | PM Peak Period <br> Counts $^{\mathbf{A}}$ | 24-Hour Counts <br> Mid-block Counts |
| :--- | :---: | :---: | :---: |
| Lantz Connector / Hwy 102 SB Ramps | Nov 17, 2022 | Nov 22,2022 | - |
| Lantz Connector / Hwy 102 NB Ramps | Nov 17, 2022 | Nov 22,2022 | - |
| Lantz Connector / Trunk 2 | Nov 15, 2022 | Nov 15, 2022 | - |
| Trunk 2 / Robert Scott Drive | Nov 14,2022 | Nov 14,2022 | - |

A - Intersection counts included separate recordings for cars/light trucks, single-unit trucks/busses, large truck/trailer combinations, bicycles, and pedestrians.

Our review of the current 2022 travel demand recorded by GRIFFIN suggested these volumes were reasonable and representative of typical late fall vehicle travel. However, the Baseline year selected for this study was 2023. Therefore, GRIFFIN elected to apply the following traffic volume adjustment factors to establish the baseline vehicle demand:

- General growth rate to increase volumes from 2022 to 2023 at a rate of $0.5 \%$ per year. This rate is consistent with the background growth rate discussed later in the report, and
- A seasonal adjustment factor using NSDPW's published 2018 factors for Trunk 2 - an " $A$ " class roadway. The timing of our data collection was consistent with NSDPW's weeks \#47 and \#48 and so volumes were increased by a factor of 1.04.

The final set of 2023 Baseline weekday AM and PM peak hour volumes applied to our analysis is contained in Figure 2.

### 2.3 Baseline 2023 Intersection Assessment

An intersection capacity analysis process was carried out using the Baseline 2023 traffic volumes (Figure 2) as well as the existing lane configurations and traffic control at the following intersections:

1. Lantz Connector Rd / Hwy 102 Southbound Ramps
2. Lantz Connector Rd / Hwy 102 Northbound Ramps
3. Lantz Connector Rd / Shaw Drive
4. Lantz Connector Rd / Trunk 2
5. Trunk 2 / Wickwire South Street (future street connection)
6. Trunk 2 / Robert Scott Drive

The analysis process used Trafficware's Synchro 11 software tool following the Transportation Research Board's Highway Capacity Manual (HCM) methodology for unsignalized intersections, as well as The Transportation Research Laboratory's (TRL) Arcady 10 software tool for modern roundabouts. The results for the five existing intersections have been summarized in Table 2. An expanded summary of results are provided in Appendix IV. Following NSDPW TIS guidelines, the measures of effectiveness used to describe the operational performance of the intersections included the Level of service (LOS), average vehicle delay, volume-to-capacity ratio (v/c ratio) and 95th percentile queue length (metres) for each movement at each of the study area intersections.

Figure 2: Baseline 2023 Peak Hour Volumes


Table 2: Baseline Intersection Operational Analysis Results

| \#1: Lantz Connector / Hwy 102 SB Ramps |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM Peak Hour |  |  | PM Peak Hour |  |  |
|  | Approach: LOS (Delay) | v/c | Queue ${ }^{\text {A }}$ | Approach: LOS (Delay) | v/c | Queue ${ }^{\text {A }}$ |
| Existing 2023 <br> roundabout existing lanes | EB Entry: n/a <br> WB Entry: A (3.6s) <br> NB Entry: n/a <br> SB Entry: A (3.5s) | $\begin{gathered} 0.17 \\ - \\ 0.06 \end{gathered}$ | $\begin{gathered} <10 \mathrm{~m} \\ - \\ <10 \mathrm{~m} \end{gathered}$ | EB Entry: $\mathrm{n} / \mathrm{a}$ <br> WB Entry: A (3.4s) <br> NB Entry: n/a <br> SB Entry: A (3.4s) | $\begin{gathered} 0.11 \\ - \\ 0.07 \end{gathered}$ | $\begin{gathered} <10 \mathrm{~m} \\ - \\ <10 \mathrm{~m} \end{gathered}$ |

## \#2: Lantz Connector / Hwy 102 NB Ramps

|  | AM Peak Hour |  | PM Peak Hour |  |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
|  | Approach: LOS <br> (Delay) | V/C | Queue $^{\mathrm{A}}$ | Approach: LOS <br> (Delay) | V/C | Queue $^{\mathrm{A}}$ |
|  | EB Entry: A (3.1s) | 0.05 | $<10 \mathrm{~m}$ | EB Entry: A (3.2s) | 0.06 | $<10 \mathrm{~m}$ |
| roundabout | WB Entry: A (3.6s) | 0.17 | $<10 \mathrm{~m}$ | WB Entry: A (3.4s) | 0.11 | $<10 \mathrm{~m}$ |
| existing lanes | NB Entry: A (3.1s) | 0.01 | $<10 \mathrm{~m}$ | NB Entry: A (3.1s) | 0.01 | $<10 \mathrm{~m}$ |
|  | SB Entry: $\mathrm{n} / \mathrm{a}$ | - | - | SB Entry: $\mathrm{n} / \mathrm{a}$ | - | - |

\#3: Lantz Connector / Shaw Drive

|  | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {A }}$ | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {A }}$ |
| Existing 2023 <br> Roundabout existing lanes | EB Entry: n/a WB Entry: n/a NB Entry: n/a SB Entry: n/a |  |  | EB Entry: n/a <br> WB Entry: n/a <br> NB Entry: n/a <br> SB Entry: n/a |  |  |

\#4: Lantz Connector / Trunk 2

|  | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
|  | Approach: LOS <br> (Delay) | V/C | Queue $^{\text {A }}$ | Approach: LOS <br> (Delay) | V/C | Queue $^{\text {A }}$ |
|  | EB Entry: A (2.0s) | 0.08 | $<10 \mathrm{~m}$ | EB Entry: A (2.3s) | 0.21 | 10 m |
| Existing 2023 | EB |  |  |  |  |  |
| roundabout | WB Entry: A (3.4s) | 0.01 | $<10 \mathrm{~m}$ | WB Entry: A (4.3s) | 0.03 | $<10 \mathrm{~m}$ |
| existing lanes | NB Entry: A (1.9s) | 0.10 | $<10 \mathrm{~m}$ | NB Entry: A (2.3s) | 0.16 | $<10 \mathrm{~m}$ |
|  | SB Entry: A (2.7s) | 0.26 | 10 m | SB Entry: A (2.4s) | 0.17 | $<10 \mathrm{~m}$ |

[^2]Table 2 - continued
\#6: Trunk 2 / Robert Scott Dr

|  | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {A }}$ | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {A }}$ |
| Existing 2023 <br> Stop-control existing lanes | NB Th-Rt: $n / a^{B}$ <br> SB Left: A (7.4s) <br> WB Lt-Rt: B (10.0s) | $\begin{aligned} & 0.01 \\ & 0.04 \end{aligned}$ | $\begin{gathered} 0 \mathrm{~m} \\ <10 \mathrm{~m} \end{gathered}$ | NB Th-Rt: $n / a^{B}$ <br> SB Left: A (7.6s) <br> WB Lt-Rt: B (10.1s) | $\begin{aligned} & 0.01 \\ & 0.02 \end{aligned}$ | $\begin{gathered} 0 \mathrm{~m} \\ <10 \mathrm{~m} \end{gathered}$ |

A - Queue represents the calculated vehicle queue length in metres occurring 95\% of the time (95 ${ }^{\text {th }}$ percentile).
B - HCM methodology assumes no delay for this first order intersection movement. No results calculated.

The analysis results contained in Table 2 suggest the existing study area intersections operate during peak periods with average delays of 10 seconds per vehicle or less, and volume to capacity ratios of 0.26 or less. The vehicle queue lengths at all study area intersections are considered to be negligible.

Generally, the calculated results appeared to be consistent with the operating conditions, driver delays, and queue lengths observed during the field review. The operational results indicate there is a considerable amount of residual capacity for all movements at the study area intersections.

## 3. FUTURE COMMUNITY GROWTH

This chapter summarizes previous community growth forecasts for the Lantz area of MEH.

### 3.1 Past Travel Demand Studies

In 2017, GRIFFIN was engaged by the NS Department of Public Works to complete the Elmsdale/Lantz Area Travel Demand Study. The main objective of this work was to review the expected population and employment growth in the MEH's Regional Service Boundary (RSB) area, and use this information to establish the future roadway capacity needed to accommodate the expected growth in travel demand ${ }^{1}$. At the time, the MEH had completed a Water Servicing study (2013) and estimated that up to 3,023 new residential units could occur within the RSB. However, the Water Servicing study was based on full build-out, long-term projections (i.e. an unlimited growth scenario). The 2017 travel demand study took a slightly different approach to the growth forecasting process. Industry best practices for transportation studies were followed and it was determined that a likely growth scenario was about 2,000 new residential units would be built in the RSB by the 2041 planning horizon - an average of about 80 units/year.

Building on our earlier work, GRIFFIN gathered and reviewed new information that was available to us for this current study, which helped to establish an updated and more recent picture regarding the full development potential within the MEH's RSB area. A summary of this information is provided in Table 3.

Table 3: Future Potential Growth in MEH's Regional Service Boundary Area

| Study Name | Full Growth Potential <br> New Residential Units |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
| MEH Water Servicing Study (2013) | $\mathbf{3 , 0 2 3}$ units |  |  |  |
| New Study Area Developments (since 2017): |  |  |  |  |
| Lantz North (Wickwire Station) TIS (2019) | 2,115 units |  |  |  |
| Lantz South TIS (2020) | 1,241 units |  |  |  |
| Enland / Elegant Acreage TIS (2021) | 500 units |  |  |  |
| FH Development Milford TIS (2022) | $\mathbf{1 , 5 5 1}$ units |  |  |  |
| TOTAL |  |  |  | $\mathbf{5 , 4 0 7}$ units |

Since the earlier studies in 2013 and 2017 were completed, several large residential neighbourhoods are now being planned in the Lantz-East Milford area and the latest combined total development of all new residential units has increased to about 5,400 units. This latest information assumes nearly 2,400 more residential units than previously contemplated by the MEH. However, it should be noted that the full development of all 5,400 units will occur over a very long time, far beyond the typical 20-25 year planning horizon used in transportation planning

[^3]studies. Thus, for the purposes of this traffic impact study a shorter planning horizon will be used, along with a corresponding reduced number of residential units likely to occur in that timeframe.

### 3.2 Community Growth on a Yearly Basis

### 3.2.1 - Recent Growth Patterns

GRIFFIN's 2017 travel demand study established a 25-year average growth estimate that was used to create traffic forecasts for the 2041 planning horizon (2016 to 2041). Looking at several source documents, GRIFFIN determined that a reasonable above-average residential growth within the MEH's Regional Service Boundary would result in a long-term average of about 80 new units per year. Therefore, the expected growth in this area of the MEH was assumed to be 400 new residential units by the 2021 planning horizon, and 2,000 new units by the 2041 planning horizon. Again, this rate of growth formed the basis of the traffic forecasts in the 2017 study.

To help understand what has actually changed since 2017, GRIFFIN carried out a comparative review of peak hour volumes at the Trunk 2 / Lantz Connector intersection. Since travel demand growth correlates well with population and employment growth, GRIFFIN measured the current peak hour travel demand and compared the following information:

- 2021 Horizon (Predicted): Forecast 2021 volumes from GRIFFIN's 2017 study report (assuming 400 new units were built between 2017 and 2021), and
- 2022 Horizon (Actual): Observed volumes recorded by GRIFFIN in November 2022

These two scenarios were selected as they both had a common road network that included the new Lantz interchange and Lantz Connector Road. The comparison of both sets of peak hour volumes at the Trunk 2 / Lantz Connector Road intersection has been provided in Figure 3.

Figure 3: Comparison of Previously Forecast 2021 and Observed 2022 Peak Hour Volumes


The comparison between the observed 2022 volumes (actual) versus GRIFFIN's forecast 2021 volumes (as predicted in our 2017 study report) shows that the current 2022 traffic demand is lower than was previously forecast. For example, current two-way volumes on Trunk 2 north of the new Lantz Connector Road are about 150 vph below the previously forecast 2021 volumes ${ }^{2}$. This could be due in part to several factors, but it appears to suggest that actual residential growth did not reach the estimated 80 new units / year, between 2017 and 2022. This is plausible given the restrictions and material shortages that plagued the building industry throughout the COVID19 pandemic.

### 3.2.2 - New Future Growth Assumptions

Recent government initiatives have committed to increasing the housing inventory in the province. This combined with the interest in private developments in the Lantz area, leads us to reconsider our previous residential growth assumptions. It is expected there will be more housing units completed in the RSB within a 20 -year horizon, and thus, the average yearly rate of development will also increase. A summary of the original and current development rates between the 2017 and 2043 planning horizons are summarized in Table 4.

Table 4: Future 20-Year Residential Growth Forecasts

| Horizon Years | Original 2017 Study |  | Current Estimate $^{2}$ |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Units/Year | Total Units $^{\mathbf{A}}$ | Units/Year | Total Units $^{\mathbf{A}}$ |
| 2017-2021 (5-year) | 80 | 400 | 50 | 300 |
| 20-year (2041) | 80 | 2,000 | - | - |
| New 20-year (2043) | - | - | 110 | 2,600 |
| AVERAGE | 80 units/yr |  | $\mathbf{9 6}$ units/yr |  |

A - cumulative total residential units.
In summary, GRIFFIN now expects a total of about 2,609 units will be built within the RSB, and in the Lantz area, between 2017 and 2043. This is an increase of about 600 units, over and above what was contemplated in the 2017 Study. On average, this equates to an increase of about 96 units/year for the Lantz area out to a 2043 horizon year.

GRIFFIN has applied this information to this current TIS process and has assumed that 2,609 new units would be built in the study area between 2023 and 2043. Further discussions of our background traffic assumptions applied to this study are provided in Section 5.

[^4]
## 4. THE PROPOSED DEVELOPMENT

This chapter describes the proposed changes to the property, and the type/magnitude of the proposed development lands.

### 4.1 A Mixed Use Neighbourhood

### 4.1.1 - Project Overview

The proposed site layout is contained in Figure 4, and includes the proposed internal roadway network needed to accommodate the full build-out of the development.

Figure 4: Conceptual Site Plan and Internal Street Layout


Source: DesignPoint
Table 5: Proposed Development Mix by Land Use Type

| Land Use Category | Residential Unit Type | Development Size |  |  |  |
| :---: | :--- | :---: | :---: | :---: | :---: |
| Residential | Detached Homes (R-1) | 371 units |  |  |  |
|  | Semi-detached Homes (R-2) | 166 units |  |  |  |
|  | Townhomes (R-3) | 252 units |  |  |  |
|  | Apartments / Multi-units (R-4) | 762 units |  |  |  |
| Residential Sub-Total |  |  |  |  | $\mathbf{1 , 5 5 1}$ units |
| Commercial | Parcel B - General office space | $21,000 \mathrm{ft}^{2}$ |  |  |  |
|  | Parcel B - Medical/Dental space | $21,000 \mathrm{ft}^{2}$ |  |  |  |
|  | Parcel D - Quick serve restaurant | $3,000 \mathrm{ft}^{2}$ |  |  |  |
|  | Parcel D - Coffee shop with drive thru | $\mathbf{2 , 0 0 0 \mathrm { ft } ^ { 2 }}$ |  |  |  |
|  | Parcel D - Gas/Convenience/Car wash | 6 fuel positions |  |  |  |
|  | Parcel F - Ground floor commercial | $\mathrm{n} / \mathrm{a}^{\mathrm{A}}$ |  |  |  |
| Commercial Sub-Total |  |  |  | $\mathbf{4 7 , 0 0 0} \mathrm{ft}^{\mathbf{2}}$ |  |

A -trip rates for ground floor commercial space in a residential apartment building are captured in residential trip rate.

The land use categories and magnitude of development for the full build out development scenario is summarized in Table 5.

### 4.1.2 - Phase 1 Development Details

A more detailed illustration of the Phase 1 development concept is provided in Figure 5. As shown, there are a number of large land parcels that will include multi-unit residential buildings (Parcels C, E, and F), commercial buildings (Parcel B), and highway commercial businesses (Parcel D). Parcel F will contain a small amount of ground floor commercial space within a multi-unit building.

Figure 5: Proposed Phase 1 Concept Plan


The primary vehicle access will be provided via the intersection formed between Trunk 2 and the new Road A. There are also three large land parcels with frontage along Trunk 2 and we have made the following access assumptions in our analysis steps:

- Parcel F: One new driveway connection to Trunk 2.
- Parcel B: One new driveway connection to Trunk 2.
- Parcel D: One new driveway connection to Road A only.


### 4.1.3 - Phase 2 Development Details

The proposed Phase 2 development details are contained in Figure 6. As shown, vehicle access will be provided via Road B (to Trunk 2) as well as two new collector street connections to the future Wickwire residential development to the south.

Figure 6: Proposed Phase 2 Concept Plan


Drivers moving to/from Phase 2 have multiple options to get to Trunk 2. To the east, drivers can use the new Road B-Road A route through Phase 1, or they can travel to the south through the future Wickwire residential development. It should also be noted no west road connection is proposed to connect with Phase 3. However, the proponent has plans to provide an Active Transportation connection across Barney's Brook to offer some mobility between these Phases.

### 4.1.4 - Phase 3 Development Details

The proposed Phase 3 development details are contained in Figure 7. As shown, vehicle access will only be provided via Roads I and J to the future Wickwire residential development to the south. No road connections are proposed to connect with Phase 2.

Figure 7: Proposed Phase 3 Concept Plan


Drivers moving to/from Phase 3 have limited options to get to Trunk 2. There is no east road connection to Phases 1 and 2 so drivers will need to travel to the south through the future Wickwire residential development. The proponent has plans to provide an Active Transportation connection across Barney's Brook to connect with Phase 2.

### 4.2 Vehicle Trip Generation Summary - Full Build-out

### 4.2.1 Overview

Currently, the subject lands are undeveloped and are generally covered with vegetation. Based on our discussions with FH Development, the 1,551 -unit residential and $47,000 \mathrm{ft}^{2}$ of neighbourhood commercial space, is likely to be constructed in phases and will contain a mix of unit types. However, our assessment has only focused on the ultimate future full build-out of the entire development. A summary of our vehicle trip generation calculations for a full build-out scenario are provided below, including separate discussions for the residential and commercial land use types.

### 4.2.2 Residential Land Use Vehicle Trip Generation

The expected site-generated vehicle trips associated with the proposed 1,551-unit residential development are summarized in Table 6. Based on GRIFFIN's past experience with large-scale residential and Mixed Use developments it appeared appropriate to apply the Institute of Transportation Engineer's (ITE) latest vehicle trip generation rates to this development. As such, the ITE's Trip Generation Manual, $11^{\text {th }}$ Edition document was applied.

The total forecast vehicle trips associated with the residential land uses during the peak hours of a typical weekday are expected to be:

- AM Peak Hour: 752 two-way trips, including 181 inbound and 571 outbound from the site.
- PM Peak Hour: 864 two-way trips, including 535 inbound and 329 outbound from the site.

To utilize conservative trip generation estimates in this study, it was assumed there would be no reduction in the residential site-generated vehicle trips associated with pass-by trips. Therefore, all calculated site generated trips were assumed to be new vehicles added to the study area road network.

Table 6: Residential Peak Hour Site-Generated Vehicle Trips - Full Build-out (vph)

|  | Size | Vehicle <br> Trip Rate | Inbound (vph) | Outbound (vph) | Total Trips (vph) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak Hour |  |  |  |  |  |
| Detached Housing: <br> Single-Family Detached Housing (ITE Code 210) | 371 units | 0.66 / unit ${ }^{\text {A }}$ | $\begin{gathered} 62 \\ (25 \%) \end{gathered}$ | $\begin{gathered} 184 \\ (75 \%) \end{gathered}$ | 246 |
| Semi-detached Housing: Single-Family Attached Housing (ITE Code 215) | 166 units | 0.49 / unit ${ }^{\text {A }}$ | $\begin{gathered} 20 \\ (25 \%) \end{gathered}$ | $\begin{gathered} 61 \\ (75 \%) \end{gathered}$ | 81 |
| Townhomes: <br> Multifamily Housing (Low-Rise) (ITE Code 220) | 252 units | 0.40 / unit ${ }^{\text {A }}$ | $\begin{gathered} 24 \\ (24 \%) \end{gathered}$ | $\begin{gathered} 77 \\ (76 \%) \end{gathered}$ | 101 |
| Apartments: <br> Multifamily Housing (Mid-Rise) <br> (ITE Code 221) | 762 units | 0.43 / unit ${ }^{\text {A }}$ | $\begin{gathered} 75 \\ (23 \%) \end{gathered}$ | $\begin{gathered} 249 \\ (77 \%) \end{gathered}$ | 324 |
| AM Peak Vehicle Trips |  |  | 181 | 571 | 752 |
| PM Peak Hour |  |  |  |  |  |
| Detached Housing: Single-Family Detached Housing (ITE Code 210) | 371 units | 0.92 / unit ${ }^{\text {A }}$ | $\begin{gathered} 215 \\ (63 \%) \end{gathered}$ | $\begin{gathered} 126 \\ (37 \%) \end{gathered}$ | 341 |
| Semi-detached Housing: <br> Single-Family Attached Housing (ITE Code 215) | 166 units | $0.58 /$ unit $^{\text {A }}$ | $\begin{gathered} 57 \\ (59 \%) \end{gathered}$ | $\begin{gathered} 39 \\ (41 \%) \end{gathered}$ | 96 |
| Townhomes: <br> Multifamily Housing (Low-Rise) <br> (ITE Code 220) | 252 units | $0.51 / u^{\text {unit }}{ }^{\text {A }}$ | $\begin{gathered} 81 \\ (63 \%) \end{gathered}$ | $\begin{gathered} 48 \\ (37 \%) \end{gathered}$ | 129 |
| Apartments: <br> Multifamily Housing (Mid-Rise) <br> (ITE Code 221) | 762 units | 0.39 / unit ${ }^{\text {A }}$ | $\begin{gathered} 182 \\ (61 \%) \end{gathered}$ | $\begin{gathered} 116 \\ (39 \%) \end{gathered}$ | 298 |
| PM Peak Vehicle Trips |  |  | 535 | 329 | 864 |

A - Rates calculated using ITE's regression formula.

### 4.2.3 Commercial Land Use Vehicle Trip Generation

The expected site-generated vehicle trips associated with the $47,000 \mathrm{ft}^{2}$ of neighbourhood commercial space being planned within the new development is summarized in Table 7. Similar to our trip generation approach presented in the previous Section, GRIFFIN determined that it was appropriate to use the Institute of Transportation Engineer's (ITE) latest vehicle trip generation rates contained in the Trip Generation Manual, $11^{\text {th }}$ Edition document. The one exception was the use of NSDPW's empirical trip rates applied to the proposed coffee shop business.

Table 7: Commercial Peak Hour Site-Generated Vehicle Trips - Full Build-out (vph)

|  | Size | Vehicle <br> Trip Rate | Inbound (vph) | Outbound (vph) | Total Trips (vph) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak Hour |  |  |  |  |  |
| Office Space: General Office (ITE Code 710) | $21,000 \mathrm{ft}^{2}$ | 2.10 / 1k ft ${ }^{2}$ | $\begin{gathered} 39 \\ (88 \%) \end{gathered}$ | $\begin{gathered} 5 \\ (12 \%) \end{gathered}$ | 44 |
| Health Centre: <br> Medical/Dental Office (ITE Code 720) | $21,000 \mathrm{ft}^{2}$ | $2.81 / 1 \mathrm{kft}{ }^{2}$ | $\begin{gathered} 47 \\ (79 \%) \end{gathered}$ | $\begin{gathered} 12 \\ (21 \%) \end{gathered}$ | 59 |
| Quick Serve Restaurant: Fast Food with Drive Thru (ITE Code 933) | 3,000 ft ${ }^{2}$ | 43.33 / 1k ft ${ }^{2}$ | $\begin{gathered} 75 \\ (58 \%) \end{gathered}$ | $\begin{gathered} 55 \\ (42 \%) \end{gathered}$ | 130 |
| Coffee Shop: <br> Coffee Shop with Drive Thru (NSDPW Trip Rates) ${ }^{\text {A }}$ | 2,000 ft ${ }^{2}$ | 123.2 / 1k ft ${ }^{2}$ | $\begin{gathered} 126 \\ (51 \%) \end{gathered}$ | $\begin{gathered} 121 \\ (49 \%) \end{gathered}$ | 247 |
| Gas Station: Gas / Convenience (ITE Code 945) | 6 fuel positions | 16.0 / fuel position | $\begin{gathered} 48 \\ (50 \%) \end{gathered}$ | $\begin{gathered} 48 \\ (50 \%) \end{gathered}$ | 96 |
| Car Wash: <br> Automated Car Wash (ITE Code 948) | 1 tunnel | 0.0 / tunnel | $\begin{gathered} 0 \\ (50 \%) \end{gathered}$ | $\begin{gathered} 0 \\ (50 \%) \end{gathered}$ | 0 |
| AM Peak Vehicle Trips |  |  | 335 | 241 | 576 |
| PM Peak Hour |  |  |  |  |  |
| Office Space: General Office (ITE Code 710) | 21,000 ft ${ }^{2}$ | 2.14 / 1k ft ${ }^{2}$ | $\begin{gathered} 8 \\ (17 \%) \end{gathered}$ | $\begin{gathered} 37 \\ (83 \%) \end{gathered}$ | 45 |
| Health Centre: <br> Medical/Dental Office (ITE Code 720) | $21,000 \mathrm{ft}^{2}$ | 3.90 / 1k ft ${ }^{2}$ | $\begin{gathered} 25 \\ (30 \%) \end{gathered}$ | $\begin{gathered} 57 \\ (70 \%) \end{gathered}$ | 82 |
| Quick Serve Restaurant: Fast Food with Drive Thru (ITE Code 933) | 3,000 ft ${ }^{2}$ | 31.33 / 1k ft ${ }^{2}$ | $\begin{gathered} 47 \\ (50 \%) \end{gathered}$ | $\begin{gathered} 47 \\ (50 \%) \end{gathered}$ | 94 |
| Coffee Shop: <br> Coffee Shop with Drive Thru (NSDPW Trip Rates) ${ }^{\text {A }}$ | 2,000 ft ${ }^{2}$ | 84.8 / 1k ft ${ }^{2}$ | $\begin{gathered} 88 \\ (52 \%) \end{gathered}$ | $\begin{gathered} 82 \\ (48 \%) \end{gathered}$ | 170 |
| Gas Station: <br> Gas / Convenience (ITE Code 945) | 6 fuel positions | 18.5 / fuel position | $\begin{gathered} 56 \\ (50 \%) \end{gathered}$ | $\begin{gathered} 55 \\ (50 \%) \end{gathered}$ | 111 |
| Car Wash: Automated Car Wash (ITE Code 948) | 1 tunnel | 14.0 / tunnel | $\begin{gathered} 7 \\ (50 \%) \end{gathered}$ | $\begin{gathered} 7 \\ (50 \%) \end{gathered}$ | 14 |
| PM Peak Vehicle Trips |  |  | 231 | 285 | 516 |

A - Vehicle trip rates provided by NSDPW for an operating Tim Hortons in Nova Scotia.

The total forecast site-generated trips associated with the commercial land uses during the peak hours of a typical weekday are expected to be:

- AM Peak Hour: 576 two-way trips, including 335 inbound and 241 outbound from the site.
- PM Peak Hour: 516 two-way trips, including 231 inbound and 285 outbound from the site.

The total vehicle trips contained in Table 7 were further divided into the three main trip types that included pass-by trips, shared trips between businesses co-located within the property, and new trips. GRIFFIN's assumed percent splits among these various trip types were based on ITE guidelines and industry best practices.

Since the majority of commercial floor space is concentrated in the Parcel B and Parcel D properties, we reviewed each parcel separately. This process allowed us to identify site-specific hared trip estimates occurring between businesses co-located within the Parcel. The assumptions applied to Parcel B are contained in Table 8, while the assumptions applied to Parcel D are contained in Table 9.

Table 8: Parcel B Commercial Land Uses - Pass-by and Shared Vehicle Trip Percentages (vph)

| Parcel B Land Use Type | Vehicle Trip Type | AM Peak Trips (two-way) | PM Peak Trips (two-way) |
| :---: | :---: | :---: | :---: |
| Office Space: General Office (ITE Code 710) | Total Trips ${ }^{\text {A }}$ | 44 | 45 |
|  | Pass-by Trips ${ }^{\text {B }}$ | 0 (0\%) | 0 (0\%) |
|  | On-site Shared Trips ${ }^{\text {c }}$ | 0 (0\%) | 0 (0\%) |
|  | New Trips | 44 | 45 |
| Health Centre: <br> Medical/Dental Office (ITE Code 720) | Total Trips ${ }^{\text {A }}$ | 59 | 82 |
|  | Pass-by Trips ${ }^{\text {B }}$ | 0 (0\%) | 0 (0\%) |
|  | On-site Shared Trips ${ }^{\text {c }}$ | 6 (10\%) | 8 (10\%) |
|  | New Trips | 53 | 74 |

A - Total trips for Parcel B taken from Table 7.
B - Pass-by trips attracted from adjacent road. Percentages based on ITE trip generation empirical surveys.
$C$ - On-site shared trips are defined as one vehicle trip that patronizes multiple businesses on-site during that one trip.
Percentages based on ITE empirical data for Mixed Use developments.

It should be noted that the "new trips" were applied to trip distribution step, discussed in Section 4.3.

Table 9: Parcel D Commercial Land Uses - Pass-by and Shared Vehicle Trip Percentages (vph)

| Parcel B Land Use Type | Vehicle Trip Type | AM Peak Trips (two-way) | PM Peak Trips (two-way) |
| :---: | :---: | :---: | :---: |
| Quick Serve Restaurant: Fast Food with Drive Thru (ITE Code 933) | Total Trips ${ }^{\text {A }}$ | 130 | 94 |
|  | Pass-by Trips ${ }^{\text {B }}$ | 40 (30\%) | 48 (50\%) |
|  | On-site Shared Trips ${ }^{\text {c }}$ | 14 (10\%) | 10 (10\%) |
|  | New Trips | 76 | 36 |
| Coffee Shop: <br> Coffee Shop with Drive Thru (NSDPW Trip Rates) | Total Trips ${ }^{\text {A }}$ | 246 | 170 |
|  | Pass-by Trips ${ }^{\text {B }}$ | 198 (80\%) | 86 (50\%) |
|  | On-site Shared Trips ${ }^{\text {c }}$ | 0 (0\%) | 0 (0\%) |
|  | New Trips | 48 | 84 |
| Gas Station: <br> Gas / Convenience (ITE Code 945) | Total Trips ${ }^{\text {A }}$ | 96 | 111 |
|  | Pass-by Trips ${ }^{\text {B }}$ | 48 (50\%) | 56 (50\%) |
|  | On-site Shared Trips ${ }^{\text {c }}$ | 10 (10\%) | 12 (10\%) |
|  | New Trips | 38 | 43 |
| Car Wash: <br> Automated Car Wash (ITE Code 948) | Total Trips ${ }^{\text {A }}$ | 0 | 14 |
|  | Pass-by Trips ${ }^{\text {B }}$ | 0 (30\%) | 4 (30\%) |
|  | On-site Shared Trips ${ }^{\text {c }}$ | 0 (50\%) | 8 (50\%) |
|  | New Trips | 0 | 2 |

A - Total trips for Parcel B taken from Table 7.
B - Pass-by trips attracted from adjacent road. Percentages based on ITE trip generation empirical surveys.
C - On-site shared trips are defined as one vehicle trip that patronizes multiple businesses on-site during that one trip.
Percentages based on ITE empirical data for Mixed Use developments.

### 4.3 Distribution of Site-Generated Trips

The distribution of new site-generated traffic requires the practitioner to correlate the origins/destinations of these trips to a point outside of the study area. Typically, the origins and destinations are located where the major roads cross the study area cordon line. In the case of this particular project, the road connections to the outer cordon line include Trunk 2 (north and south), and Highway 102 (north and south).

There were three key factors taken into consideration when developing the expected distribution patterns for each land use type. These included the following:

- The proximity of the community services located to the south in Lantz and Elmsdale;
- Access to the Highway 102 regional travel corridor via the new Lantz Connector Road; and
- A review of the current traffic flow directional splits at the Trunk 2 / Robert Scott Drive intersection.

Information and data associated with all three of these factors were reviewed and the selected distribution percentages applied to the study analyses are summarized in Table 10. As shown, GRIFFIN applied different vehicle trip distribution percentages for the residential and commercial land use types. Drivers moving to/from each of these land use types generally have different trip purposes and travel route choices.

Table 10: Site-Generated Trip Distribution by Land Use Type

| Direction | Via | Residential <br> Land Uses | Parcel B Commercial <br> Office / Health Centre | Parcel D <br> Commercial / Retail |
| :---: | :---: | :---: | :---: | :---: |
|  | Trunk 2 | $15 \%$ | $15 \%$ | $25 \%$ |
|  | Highway 102 | $5 \%$ | $5 \%$ | $0 \%$ |
| East | Route 277 | $2 \%$ | $5 \%$ | $0 \%$ |
|  | Trunk 2 | $18 \%$ | $30 \%$ | $0 \%$ |
|  | Highway 102 | n/a | $60 \%$ | $15 \%$ |
| Internal ${ }^{\mathbf{A}}$ | Internal Streets | - | - | $0 \%$ |
| Total |  |  |  |  |

A - Internal trips are assumed to be generated from within the new residential areas. For Parcels $B \& D$, trips are assigned between residential areas, along Trunk 2, to the Parcel driveways.

It should be noted that a portion of the site-generated trips are assumed to only occur internally within the development. This assumption is based on the expectation that some residents will travel between their residence to patronize one of the new commercial businesses, for example. Although we refer to these trips as "internal", they were still explicitly considered and added to the Trunk 2 volumes as well as the driveway volumes for Parcels B and D. This is discussed in more detail in the following Section.

### 4.4 Street Connections and Vehicle Trip Assignment

### 4.4.1 Overview of Assignment Process

The assignment of vehicle trips associated with a new development is the process of distributing the site-generated trips across multiple routes between each set of origin and destination pairs. For example, if a retail business had multiple driveways then drivers have a choice to move in/out of both driveways as they travel to/from the north, the south, and so forth.

For this particular study, the vehicle trip assignment process utilized multiple connection options to access the Trunk 2 corridor. The expected demand assigned to each Trunk 2 access point was based on the proximity and relative convenience to each Phase and sub-area within the proposed development. Further, there are multiple internal street connections for Phases 1 and 2; however, Phase 3 has no internal connectivity and must utilize the Wickwire Development internal street system to gain access to Trunk 2.

### 4.4.2 Assignment of Residential Trips

The trip assignment process for the residential land uses required additional assessment and rationalization. The residential-based trips were assigned to the three new street connections (i.e. Road A, Wickwire North, and Wickwire South) based on the proximity and relative convenience for the new residents. Our assumed assignment of residential trips to each new Trunk 2 intersection is contained in Table 11.

Table 11: Vehicle Trip Assignment Percentages

|  | New Road A | Wickwire North <br> Street | Wickwire South <br> Street | Total Percent |
| :---: | :---: | :---: | :---: | :---: |
| Percent Assigned <br> Trips | $58 \%$ | $32 \%$ | $10 \%$ | $100 \%$ |

The results of the assignment process for the new site-generated residential trips are shown graphically in Figure 8.

### 4.4.3 Assignment of Commercial Trips

Since there are no internal roadway connections between the new residential areas and Parcels B, D, and F, GRIFFIN explicitly assigned all commercial trips generated by these Parcels to/from the Trunk 2 corridor using the distribution percentages contained in Table 10.

The "internal" trips were explicitly added to the Parcel driveways, Trunk 2 corridor, and the intersections offering access to the proposed development (eg. Road A). These trips were also included in our intersection evaluations discussed later in this report. The majority of these "internal" commercial trips were assigned in/out of Road A which corresponds with the Phase 1 and Phase 2 residential areas. Since the Phase 3 residential area has no opportunity to connect internally to Road A, we assigned these trips via the Wickwire street connections to Trunk 2.

The assignment of all commercial trips are shown graphically in Figure 9.

Figure 8: Site-Generated Peak Hour Volumes - Residential Land Uses


Figure 9: Site-Generated Peak Hour Volumes - Commercial Land Uses


## 5. DEVELOPING FUTURE TRAFFIC VOLUMES

This chapter summarizes the process and assumptions used to develop the future year traffic volumes expected by the 2043 planning horizon.

### 5.1 Overview

The future planning horizon chosen for a traffic impact study represents a milestone in the development process. Following NSDPW guidelines, the future planning horizon year used in the analysis for this type of development will occur 5 years beyond the expected full buildout/occupancy of the site.

Through discussions with FH Development, it was determined that the full build-out of the subject lands will be dependent on market demands as individual lots are purchased. In recent years, the rate of population growth in this area of the Province has been moderate. Thus, it appeared reasonable to take a longer-term outlook for the 1,551-unit development to fully develop. GRIFFIN has assumed the full build-out timeframe for this Mixed Use neighbourhood would be about 12-15 years, plus an addition 5 year timeframe required by NSDPW. Using these expected timelines GRIFFIN has provided a summary of the planning horizon assumptions in Table 12.

Table 12: Development Completion Dates and Study Horizon Years

| Planning <br> Horizons | Development / Traffic Scenario | Roadway Network |
| :---: | :---: | :---: |
| 2023 Planning Horizon | 2023 Existing Conditions | Existing roadway network (with Lantz Interchange) |
| 2043 Planning Horizon | 2043 Future Background Conditions: <br> - Lantz South (30\% complete, 373 units) <br> - Lantz North (30\% complete, 635 units) <br> - Enland/Elegant Acreage (10\% complete, 50 units) <br> - These development rates equate to 1,058 new residential units. | Existing roadway network (with Lantz Interchange) |
|  | 2043 Future Total - Development Scenario 1: <br> - The above-noted Background development assumptions (1,058 units), plus <br> - Full build-out of the proposed FH Development's Milford development (1,551 units) | Existing roadway network (with Lantz Interchange) |
|  | 2043 - Sensitivity Assessment of Trunk 2 Corridor: <br> - Full build-out of the FH Development's East Milford development (1,551 units), plus <br> - Full build-out of Armco's Wickwire development (2,115 units) <br> - This scenario includes a total of 3,666 units. | Analysis focused only on three new intersections along Trunk 2 |

Following traffic impact study best practices, the analysis process carried out for the future planning horizon includes two sets of assessments. The first is referred to as the future background traffic scenario which excludes the proposed site-generated traffic (i.e., future status quo). The second is referred to as the future total traffic scenario which adds the proposed sitegenerated traffic to the street network. It is through this process that the practitioner can identify the impacts explicitly associated with the new site-generate traffic added to the roadway network by comparing the two sets of results, presented in Section 6. Specific to this study, the NSDPW has requested that an additional future development scenario be evaluated - which we refer to as a sensitivity assessment - and the results of this additional evaluation is presented later in Section 8.

The assembly of both sets of future 2043 peak hour traffic volumes is discussed in the following Sections.

### 5.2 Future Background Traffic Volumes

### 5.2.1 Component \#1 - General Traffic Growth

Developing future "background" traffic volumes typically consists of general traffic growth, any future planned developments, and any planned road network changes in the vicinity of the study area. To establish a reasonable general background traffic growth rate for this area, GRIFFIN reviewed historical NSDPW traffic volumed data along Trunk 2 as well as the assumptions made in the 2017 Elmsdale-Lantz Travel Demand Modelling Study. Average Annual Daily Traffic (AADT) volumes recorded by NSDPW between 2009 and 2017 showed a $0.42 \%$ per year increase over this period. Therefore, a slightly higher-than-average compounding growth rate of $0.5 \%$ per year was applied to the 2023 Baseline volumes. This rate is consistent with assumptions made in previous traffic studies for this area. The explicit impacts associated with the larger developments are discussed below.

### 5.2.2 Component \#2 - Road Network Changes

When the roadway network is changed or modified at some point between the Baseline year and the future planning horizon, there is a potential for traffic flow patterns to change. For this study; however, the road network is not expected to change and was assumed to remain the same out to the 2043 planning horizon.

### 5.2.3 Component \#3 - Adjacent Developments

Since 2019, several major residential developments have initiated planning approval processes with the MEH. These developments were discussed earlier in this report, and we provide a summary of their development magnitude in Table 13.

Table 13: Summary of Background Developments

| Development Name | $\begin{aligned} & \text { TIS } \\ & \text { Year } \end{aligned}$ | 100\% Build-out |  | 2043 Build-out (estimate) |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\begin{aligned} & \text { Residential } \\ & \text { (units) } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { Commercial } \\ & \left(\mathrm{ft}^{2}\right) \end{aligned}$ | Residential (units) | $\begin{gathered} \text { Commercial } \\ \left(\mathrm{ft}^{2}\right) \end{gathered}$ |
| 1 - Lantz North / Wickwire Station | 2019 | 2,115 | 50,000 | 635 (30\%) | 15,000 (30\%) |
| 2 - Lantz South | 2020 | 1,241 | 220,100 | 373 (30\%) | 66,030 (30\%) |
| 3 - Enland / Elegant Acreage | 2021 | 500 | ${ }^{-}$ | 50 (10\%) | - |
|  | TOTALS | 3,856 units | 270,100 ft ${ }^{\text {2 }}$ | 1,058 units | 66,045 ft ${ }^{\text {2 }}$ |

Therefore, the development of background traffic for the 2043 planning horizon used in this current study was comprised of the following:

- Traffic growth from 2023 to 2043 using a $0.50 \%$ compounding rate (a 1.105 factor), and
- 30\% of the Lantz North / Wickwire Development site-generated traffic, and
- $30 \%$ of the Lantz South Development site-generated traffic, and
- $10 \%$ of the Enland / Elegant Acreage Development site-generated traffic.

For each background development, GRIFFIN referenced the site-generated vehicle trips from their respective TIS study reports. However, GRIFFIN adjusted the trip distribution and assignment patterns slightly to reflect actual traffic flow patterns observed during November 2022 - with the new Lantz Connector Road and new interchange open and operational. This approach provided a more accurate representation of future traffic flow conditions.

The resulting future Background 2043 peak hour volumes are contained in Figure 10.

### 5.3 Future Total Traffic Volumes - Development Scenario 1

Under the future Total 2043 traffic scenario, the proposed development is expected to be fully constructed and occupied. The traffic volumes for this scenario were developed using the following assumptions:

- Future background 2043 volumes (Figure 10), plus
- $\quad$ Site-generated traffic volumes (Figures 8 and 9).

The future Total 2043 traffic volumes used in the analysis are shown in Figure 11.

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Figure 10: Future Background 2043 Peak Hour Volumes


Figure 11: Future Total 2043 Peak Hour Volumes - Development Scenario 1


## 6. FUTURE 2043 TRAFFIC OPERATIONAL ANALYSIS

This chapter summarizes the results of the future year traffic operations analysis, including the auxiliary turn lane warrants, and intersection capacity review at the 2043 Horizon.

### 6.1 Analysis Step \#1 - Traffic Signal Warrant Review

The initial step in the analysis process identified the need for signalized traffic control by using the Transportation Association of Canada's (TAC) signal warrant procedure. This methodology is widely used by road agencies across Canada and is a recognized procedure by the NSDPW. The TAC calculation process uses a set of average intersection volumes measured over the six highest hours of a typical day. The results of this calculation process include a number of priority points to indicate whether a traffic signal is warranted. When the minor street traffic volume exceeds 75 vehicles/hour and the number of priority points exceeds 100 , the traffic signal warrant is met.

GRIFFIN used the observed November 2022 hourly traffic volume profile recorded at the Trunk 2 / Lantz Connector Road intersection to establish the temporal profile and identify the six highest hours. These data were considered to be representative of current study area traffic flow patterns and were applied to the TAC warrant calculations. The results are contained in Table 14. Detailed signal warrant assessments are contained in Appendix II.

Table 14: Summary of Traffic Signal Warrant Results

| Intersection No. \& Location | Development Scenarios |  |  |
| :---: | :---: | :---: | :---: |
|  | Baseline 2023 | Background 2043 | Total 2043 |
| \#6: Trunk 2 / Robert Scott-Wickwire |  |  |  |
| North St | $\mathrm{n} / \mathrm{a}^{\mathrm{A}}$ | 38 points | $\mathbf{1 3 8}$ points |
| \#7: Trunk 2 / New Road A | $\mathrm{n} / \mathrm{a}^{\mathrm{A}}$ | 13 points $^{\mathrm{B}}$ | 76 points ${ }^{\mathrm{B}}$ |
| \#8: Trunk 2 / Parcel B <br> Commercial Access | $\mathrm{n} / \mathrm{a}^{\mathrm{A}}$ | $\mathrm{n} / \mathrm{a}^{\mathrm{A}}$ | 76 points |
| \#9: Trunk 2 / Parcel F <br> Residential Access | $\mathrm{n} / \mathrm{a}^{\mathrm{A}}$ | $\mathrm{n} / \mathrm{a}^{\mathrm{A}}$ | 19 points |
| \#10: Road A / Parcel D <br> Commercial Access | $\mathrm{n} / \mathrm{a}^{\mathrm{A}}$ | $\mathrm{n} / \mathrm{a}^{\mathrm{A}}$ | 18 points |

[^5]The results contained in Table 14 suggest only one future intersection will require a traffic control upgrade from stop-control to either signalization or a roundabout - the Wickwire South intersection. The overall findings include:

- Trunk 2 / Wickwire South Street: This three-leg intersection is expected to require either traffic signals or a roundabout to accommodate the assumed development rates by the 2043 planning horizon.
- Trunk 2 / Robert Scott-Wickwire South Street: This intersection can operate with stopcontrol under our assumed Total 2043 peak hour traffic demand. However, with more growth to occur within the future Wickwire development there will likely be a need for traffic signals at some point in the future.
- Trunk 2 / New Road A: This future intersection can accommodate the majority of the proposed Phase 1 and a portion of the Phase 2 traffic. Under a full buildout scenario (i.e. 1,551 units) this intersection is expected to function adequately with stop-control.

Our results also indicate that all new intersections and accesses associated with the proposed Mixed Use development can operate with unsignalized traffic control under the assumed Total 2043 peak hour traffic demand. These signal warrant results were carried forward to the intersection performance analysis presented in Section 6.3.

### 6.2 Analysis Step \#2 - Auxiliary Turn Lane Review

The next step in the analysis process included a review of the auxiliary turn lane needs at the unsignalized, stop-controlled intersections included in this study. Since the Lantz Connector Road corridor is comprised of four modern roundabouts, the focus of our review shifted to the Trunk 2 corridor.

The left turn lane warrant review followed Ministry of Transportation of Ontario (MTO) procedures. The right turn lane warrant review followed the Ohio Department of Transportation (ODOT) methodology. A summary of the auxiliary turn lane assessment results are provided in Table 15. Detailed auxiliary turn lane warrant assessments are contained in Appendix III.

Under the assumed future Total 2043 peak hour conditions we can expect the need for left turn lanes in the following locations:

- On Trunk 2 at the Robert Scott Drive-Wickwire North Street unsignalized intersection, and
- On Trunk 2 at the new Road A unsignalized intersection, and
- On Road A at the new Parcel D highway commercial access - assuming only one access.

The auxiliary turn lane warrant assessment results indicate that auxiliary right turn lanes are not required at any unsignalized intersection in the study area. These results have been carried forward to the intersection performance assessment discussed in the next Section.

Table 15: Summary of Auxiliary Turn Lane Assessments

| Intersection No. \& Location | Turn Lane | Development Scenarios |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  | Baseline 2023 | Background 2043 | Total 2043 |
| \#5: Trunk 2 / Wickwire South St | Left Turn Lane | $n / a^{A}$ | Warrant met | signalized ${ }^{\text {B }}$ |
|  | Right Turn Lane | $n / a^{A}$ | Warrant not met | signalized $^{\text {B }}$ |
| \#6: Trunk 2 / Robert ScottWickwire North St | Left Turn Lane | Warrant not met | Warrant not met | Warrant met |
|  | Right Turn Lane | Warrant not met | Warrant not met | Warrant not met |
| \#7: Trunk 2 / New Road A | Left Turn Lane | $n / a^{A}$ | $n / a^{A}$ | Warrant met |
|  | Right Turn Lane | $n / a^{\text {A }}$ | $n / a^{\text {A }}$ | Warrant not met |
| \#8: Trunk 2 / Parcel B Commercial Access | Left Turn Lane | $n / a^{A}$ | $n / a^{A}$ | Warrant not met |
|  | Right Turn Lane | $n / a^{A}$ | $n / a^{A}$ | Warrant not met |
| \#9: Trunk 2 / Parcel F Residential Access | Left Turn Lane | $n / a^{A}$ | $n / a^{A}$ | Warrant not met |
|  | Right Turn Lane | $n / a^{A}$ | $n / a^{A}$ | Warrant not met |
| \#10: Road A / Parcel D Commercial Access | Left Turn Lane | $n / a^{A}$ | $n / a^{A}$ | Warrant met |
|  | Right Turn Lane | $n / a^{A}$ | $n / a^{A}$ | Warrant not met |

A - This intersection does not exist under this development scenario.
$B$ - Results provided only for scenarios with stop-control. Future Total scenario requires signalization, thus no results.

### 6.3 Analysis Step \#3 - Future 2043 Intersection Performance Analysis

A capacity and operational performance analysis effort was carried for each study area intersection using the future 2043 forecast traffic volumes. The analysis process used the industryaccepted Trafficware Synchro 11 software tool for signalized/unsignalized intersections, which is based on the methodologies contained in the Transportation Research Board's (TRB) Highway Capacity Manual. The evaluation of modern roundabouts was completed using the latest version of the Transportation Research Laboratory's Arcady software tool.

A summary of results for the critical intersection movements are contained in Table 16 and the detailed capacity reports are contained in Appendix IV. Following NSDPW's TIS guidelines, the measures of effectiveness used to describe the operational performance included the level of service, average vehicle delay, volume-to-capacity ratio ( $\mathrm{v} / \mathrm{c}$ ratio) and $95^{\text {th }}$ percentile queue length (metres) for all approaches to the intersection.

Table 16: Future 2043 Intersection Operational Analysis Results
\#1: Lantz Connector / Hwy 102 SB Ramps

|  | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {A }}$ | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {A }}$ |
| Existing 2023 <br> Roundabout - <br> existing lanes | EB Entry: n/a <br> WB Entry: A (3.6s) <br> NB Entry: n/a <br> SB Entry: A (3.5s) | $\begin{gathered} 0.17 \\ - \\ 0.06 \end{gathered}$ | $\begin{gathered} <10 \mathrm{~m} \\ - \\ <10 \mathrm{~m} \end{gathered}$ | EB Entry: n/a <br> WB Entry: A (3.4s) <br> NB Entry: n/a <br> SB Entry: A (3.4s) | $\begin{gathered} 0.11 \\ - \\ 0.07 \end{gathered}$ | $\begin{gathered} <10 \mathrm{~m} \\ - \\ <10 \mathrm{~m} \end{gathered}$ |
| Background 2043 <br> Roundabout existing lanes | EB Entry: n/a <br> WB Entry: A (4.7s) <br> NB Entry: $\mathrm{n} / \mathrm{a}$ <br> SB Entry: A (4.5s) | $\begin{gathered} 0.37 \\ - \\ 0.11 \end{gathered}$ | $\begin{gathered} 15 \mathrm{~m} \\ - \\ <10 \mathrm{~m} \end{gathered}$ | EB Entry: n/a <br> WB Entry: A (4.1s) <br> NB Entry: $\mathrm{n} / \mathrm{a}$ <br> SB Entry: A (4.2s) | $\begin{gathered} 0.27 \\ - \\ 0.15 \end{gathered}$ | $\begin{gathered} <10 \mathrm{~m} \\ - \\ <10 \mathrm{~m} \end{gathered}$ |
| Total 2043 <br> Roundabout existing lanes | EB Entry: n/a <br> WB Entry: A (9.2s) <br> NB Entry: $\mathrm{n} / \mathrm{a}$ <br> SB Entry: A (7.3s) | $\begin{gathered} 0.68 \\ - \\ 0.19 \end{gathered}$ | 30 m <br> 10 m | EB Entry: n/a <br> WB Entry: A (5.5s) <br> NB Entry: $\mathrm{n} / \mathrm{a}$ <br> SB Entry: A (5.6s) | $\begin{gathered} 0.46 \\ - \\ 0.22 \end{gathered}$ | $\begin{gathered} 10 \mathrm{~m} \\ - \\ 10 \mathrm{~m} \end{gathered}$ |

\#2: Lantz Connector / Hwy 102 NB Ramps

|  | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {A }}$ | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {A }}$ |
| Existing 2023 <br> Roundabout existing lanes | EB Entry: A (3.1s) <br> WB Entry: A (3.6s) <br> NB Entry: A (3.1s) <br> SB Entry: n/a | $\begin{aligned} & 0.05 \\ & 0.17 \\ & 0.01 \end{aligned}$ | $\begin{aligned} & <10 \mathrm{~m} \\ & <10 \mathrm{~m} \\ & <10 \mathrm{~m} \end{aligned}$ | EB Entry: A (3.2s) <br> WB Entry: A (3.4s) <br> NB Entry: A (3.1s) <br> SB Entry: n/a | $\begin{aligned} & 0.06 \\ & 0.11 \\ & 0.01 \end{aligned}$ | $\begin{aligned} & <10 \mathrm{~m} \\ & <10 \mathrm{~m} \\ & <10 \mathrm{~m} \end{aligned}$ |
| Background 2043 <br> Roundabout existing lanes | EB Entry: A (3.3s) <br> WB Entry: A (4.7s) <br> NB Entry: A (3.2s) <br> SB Entry: n/a | $\begin{aligned} & 0.08 \\ & 0.37 \\ & 0.01 \end{aligned}$ | $\begin{gathered} <10 \mathrm{~m} \\ 15 \mathrm{~m} \\ <10 \mathrm{~m} \end{gathered}$ | EB Entry: A (3.4s) <br> WB Entry: A (4.1s) <br> NB Entry: A (3.2s) <br> SB Entry: n/a | $\begin{aligned} & 0.12 \\ & 0.27 \\ & 0.01 \end{aligned}$ | $\begin{gathered} <10 \mathrm{~m} \\ 10 \mathrm{~m} \\ <10 \mathrm{~m} \end{gathered}$ |
| Total 2043 <br> Roundabout - <br> existing lanes | EB Entry: A (3.3s) <br> WB Entry: A (9.3s) <br> NB Entry: A (3.2s) <br> SB Entry: n/a | $\begin{aligned} & 0.09 \\ & 0.68 \\ & 0.01 \end{aligned}$ | $\begin{gathered} <10 \mathrm{~m} \\ 30 \mathrm{~m} \\ <10 \mathrm{~m} \end{gathered}$ | EB Entry: A (3.5s) <br> WB Entry: A (5.5s) <br> NB Entry: A (3.3s) <br> SB Entry: n/a | $\begin{aligned} & 0.15 \\ & 0.46 \\ & 0.01 \end{aligned}$ | $\begin{gathered} <10 \mathrm{~m} \\ 10 \mathrm{~m} \\ <10 \mathrm{~m} \end{gathered}$ |

A - Queue represents the calculated vehicle queue length in metres occurring $95 \%$ of the time ( $95^{\text {th }}$ percentile).
B - HCM methodology assumes no delay for this first order intersection movement. No results calculated.

Table 16-continued

| \#3: Lantz Connector / Shaw Drive |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM Peak Hour |  |  | PM Peak Hour |  |  |
|  | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {a }}$ | Approach: LOS (Delay) | v/C | Queue ${ }^{\text {a }}$ |
| Existing 2023 <br> Roundabout existing lanes | EB Entry: n/a <br> WB Entry: n/a <br> NB Entry: n/a <br> SB Entry: n/a |  |  | EB Entry: n/a <br> WB Entry: n/a <br> NB Entry: n/a <br> SB Entry: n/a |  |  |
| Background 2043 <br> Roundabout - <br> existing lanes | EB Entry: A (2.0s) <br> WB Entry: A (2.9s) <br> NB Entry: A (4.3s) <br> SB Entry: n/a | $\begin{aligned} & 0.12 \\ & 0.31 \\ & 0.22 \end{aligned}$ | $\begin{gathered} <10 \mathrm{~m} \\ 15 \mathrm{~m} \\ 10 \mathrm{~m} \end{gathered}$ | EB Entry: A (2.8s) <br> WB Entry: A (2.3s) <br> NB Entry: A (6.8s) <br> SB Entry: n/a | $\begin{aligned} & 0.37 \\ & 0.17 \\ & 0.33 \end{aligned}$ | $\begin{gathered} 15 \mathrm{~m} \\ <10 \mathrm{~m} \\ 15 \mathrm{~m} \end{gathered}$ |
| Total 2043 <br> Roundabout existing lanes | EB Entry: A (2.2s) <br> WB Entry: A (5.7s) <br> NB Entry: A (5.0s) <br> SB Entry: n/a | $\begin{aligned} & 0.19 \\ & 0.60 \\ & 0.25 \end{aligned}$ | $\begin{gathered} <10 \mathrm{~m} \\ 15 \mathrm{~m} \\ 10 \mathrm{~m} \end{gathered}$ | EB Entry: A (4.0s) <br> WB Entry: A (3.0s) <br> NB Entry: B (12.7s) <br> SB Entry: n/a | $\begin{aligned} & 0.56 \\ & 0.32 \\ & 0.48 \end{aligned}$ | $\begin{aligned} & 15 \mathrm{~m} \\ & 15 \mathrm{~m} \\ & 15 \mathrm{~m} \end{aligned}$ |

\#4: Lantz Connector / Trunk 2

|  | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {A }}$ | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {A }}$ |
| Existing 2023 <br> Roundabout existing lanes | EB Entry: A (2.0s) <br> WB Entry: A (3.4s) <br> NB Entry: A (1.9s) <br> SB Entry: A (2.7s) | $\begin{aligned} & 0.08 \\ & 0.01 \\ & 0.10 \\ & 0.26 \end{aligned}$ | $\begin{gathered} <10 \mathrm{~m} \\ <10 \mathrm{~m} \\ <10 \mathrm{~m} \\ 10 \mathrm{~m} \end{gathered}$ | EB Entry: A (2.3s) <br> WB Entry: A (4.3s) <br> NB Entry: A (2.3s) <br> SB Entry: A (2.4s) | $\begin{aligned} & 0.21 \\ & 0.03 \\ & 0.16 \\ & 0.17 \end{aligned}$ | $\begin{gathered} 10 \mathrm{~m} \\ <10 \mathrm{~m} \\ <10 \mathrm{~m} \\ <10 \mathrm{~m} \end{gathered}$ |
| Background 2043 <br> Roundabout - <br> existing lanes | EB Entry: A (2.2s) <br> WB Entry: A (3.7s) <br> NB Entry: A (2.1s) <br> SB Entry: A (3.7s) | $\begin{aligned} & 0.13 \\ & 0.02 \\ & 0.13 \\ & 0.45 \end{aligned}$ | $\begin{aligned} & <10 m \\ & <10 m \\ & <10 m \\ & 15 m \end{aligned}$ | EB Entry: A (2.9s) <br> WB Entry: A (5.8s) <br> NB Entry: A (2.9s) <br> SB Entry: A (2.9s) | $\begin{aligned} & 0.35 \\ & 0.04 \\ & 0.29 \\ & 0.30 \end{aligned}$ | $\begin{gathered} 15 \mathrm{~m} \\ <10 \mathrm{~m} \\ 10 \mathrm{~m} \\ 15 \mathrm{~m} \end{gathered}$ |
| Total 2043 <br> Roundabout existing lanes | EB Entry: A (2.6s) <br> WB Entry: A (4.1s) <br> NB Entry: A (2.3s) <br> SB Entry: A (7.9s) | $\begin{aligned} & 0.22 \\ & 0.02 \\ & 0.17 \\ & 0.75 \end{aligned}$ | $\begin{gathered} 10 \mathrm{~m} \\ <10 \mathrm{~m} \\ <10 \mathrm{~m} \\ 55 \mathrm{~m} \end{gathered}$ | EB Entry: A (4.5s) <br> WB Entry: B (10.2s) <br> NB Entry: A (4.2s) <br> SB Entry: A (4.0s) | $\begin{aligned} & 0.57 \\ & 0.07 \\ & 0.42 \\ & 0.49 \end{aligned}$ | $\begin{gathered} 15 \mathrm{~m} \\ <10 \mathrm{~m} \\ 15 \mathrm{~m} \\ 15 \mathrm{~m} \end{gathered}$ |

A - Queue represents the calculated vehicle queue length in metres occurring 95\% of the time (95 ${ }^{\text {th }}$ percentile).
B - HCM methodology assumes no delay for this first order intersection movement. No results calculated.

Table 16-continued

|  | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {A }}$ | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {A }}$ |
| Existing 2023 ${ }^{\text {C }}$ <br> No intersection | n/a | - | - | n/a | - | - |
| Background 2043 <br> Stop-control | SB Th-Rt: $n / a^{B}$ <br> NB Left: A (8.1s) <br> EB Left: B (13.9s) <br> EB Right: B (12.1s) | $\begin{gathered} - \\ 0.05 \\ 0.03 \\ 0.27 \end{gathered}$ | $\begin{aligned} & <10 \mathrm{~m} \\ & <10 \mathrm{~m} \\ & 10 \mathrm{~m} \end{aligned}$ | SB Th-Rt: $n / a^{B}$ <br> NB Left: A (8.3s) <br> EB Left: C (19.5s) <br> EB Right: B (10.4s) | $\begin{aligned} & 0.16 \\ & 0.05 \\ & 0.15 \end{aligned}$ | $\begin{aligned} & <10 \mathrm{~m} \\ & <10 \mathrm{~m} \\ & <10 \mathrm{~m} \end{aligned}$ |
| Total 2043 <br> Signalized | SB Entry: C (28.2s) <br> NB Entry: A (6.1s) <br> EB Entry: B (15.1s) | $\begin{aligned} & 0.88 \\ & 0.31 \\ & 0.54 \end{aligned}$ | $\begin{gathered} 190 \mathrm{~m} \\ 40 \mathrm{~m} \\ 20 \mathrm{~m} \end{gathered}$ | SB Entry: C (21.9s) <br> NB Entry: B (10.1s) <br> EB Entry: B (13.7s) | $\begin{aligned} & 0.75 \\ & 0.63 \\ & 0.35 \end{aligned}$ | $\begin{gathered} 100 \mathrm{~m} \\ 115 \mathrm{~m} \\ 20 \mathrm{~m} \end{gathered}$ |

\#6: Trunk 2 / Robert Scott Dr-Wickwire North St

|  | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {A }}$ | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {A }}$ |
| Existing 2023 <br> Stop-control existing lanes | NB Th-Rt: $n / a^{B}$ <br> SB Left: A (7.4s) <br> WB Entry: B (10.0s) <br> EB Entry: n/a | $\begin{aligned} & 0.01 \\ & 0.04 \end{aligned}$ | $\begin{gathered} 0 \mathrm{~m} \\ <10 \mathrm{~m} \end{gathered}$ | NB Th-Rt: $\mathrm{n} / \mathrm{a}^{B}$ <br> SB Left: A (7.6s) <br> WB Entry: B (10.1s) <br> EB Entry: n/a | $\begin{aligned} & 0.01 \\ & 0.02 \end{aligned}$ | $\begin{gathered} 0 \mathrm{~m} \\ <10 \mathrm{~m} \end{gathered}$ |
| Background 2043 <br> Stop-control - <br> new west leg | NB Left: A (7.7s) <br> SB Left: A (7.5s) <br> WB Entry: B (12.4s) <br> EB Entry: B (10.1s) | $\begin{aligned} & 0.02 \\ & 0.01 \\ & 0.07 \\ & 0.12 \end{aligned}$ | $\begin{gathered} <10 \mathrm{~m} \\ 0 \mathrm{~m} \\ <10 \mathrm{~m} \\ 10 \mathrm{~m} \end{gathered}$ | NB Left: A (7.7s) <br> SB Left: A (7.7s) <br> WB Entry: B (13.1s) <br> EB Entry: B (10.0s) | $\begin{aligned} & 0.06 \\ & 0.01 \\ & 0.04 \\ & 0.07 \end{aligned}$ | $\begin{gathered} <10 \mathrm{~m} \\ 0 \mathrm{~m} \\ <10 \mathrm{~m} \\ <10 \mathrm{~m} \end{gathered}$ |
| Total 2043 <br> Stop-control new west leg | NB Left: A (8.9s) <br> SB Left: A (8.0s) <br> WB Entry: F (67.2s) <br> EB Entry: C (20.9s) | $\begin{aligned} & 0.08 \\ & 0.01 \\ & 0.40 \\ & 0.55 \end{aligned}$ | $\begin{gathered} <10 \mathrm{~m} \\ 0 \mathrm{~m} \\ 15 \mathrm{~m} \\ 25 \mathrm{~m} \end{gathered}$ | NB Left: A (9.3s) <br> SB Left: A (8.6s) <br> WB Entry: F (81.1s) <br> EB Entry: C (17.9s) | $\begin{aligned} & 0.26 \\ & 0.01 \\ & 0.30 \\ & 0.37 \end{aligned}$ | 10 m <br> Om <br> 10 m <br> 15 m |

A - Queue represents the calculated vehicle queue length in metres occurring 95\% of the time (95 ${ }^{\text {th }}$ percentile).
B - HCM methodology assumes no delay for this first order intersection movement. No results calculated.
$C$ - Intersection does not exist under this scenario.

Table 16-continued
\#7: Trunk 2 / New Road A

|  | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {A }}$ | Approach: LOS (Delay) | v/C | Queue ${ }^{\text {A }}$ |
| Existing 2023 ${ }^{\text {c }}$ | n/a | - | - | n/a | - | - |
| Background 2043 ${ }^{\text {c }}$ | n/a | - | - | n/a | - | - |
| Total 2043 <br> Stop-control | SB Th-Rt: $n / a^{B}$ <br> NB Left: A (8.3s) <br> EB Left: C (21.0s) <br> EB Right: B (13.0s) | $\begin{gathered} - \\ 0.10 \\ 0.33 \\ 0.39 \end{gathered}$ | $\begin{gathered} <10 \mathrm{~m} \\ 10 \mathrm{~m} \\ 15 \mathrm{~m} \end{gathered}$ | SB Th-Rt: $n / a^{B}$ <br> NB Left: A (8.9s) <br> EB Left: E (36.9s) <br> EB Right: B (11.6s) | $\begin{aligned} & 0.21 \\ & 0.41 \\ & 0.23 \end{aligned}$ | 10m <br> 15m <br> 10m |

\#8: Trunk 2 / Parcel B Commercial Access

|  | AM Peak Hour |  | PM Peak Hour |  |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
|  | Approach: LOS <br> (Delay) | V/C | Queue $^{\mathrm{A}}$ | Approach: LOS <br> (Delay) | V/C | Queue $^{\mathrm{A}}$ |
|  | $\mathrm{n} / \mathrm{a}$ | - | - | $\mathrm{n} / \mathrm{a}$ | - | - |
| Background 2043 $^{\mathrm{C}}$ | $\mathrm{n} / \mathrm{a}$ | - | - | $\mathrm{n} / \mathrm{a}$ | - | - |
| Total 2043 | SB Th-Rt: $\mathrm{n} / \mathrm{a}^{\mathrm{B}}$ | - | - | SB Th-Rt: $\mathrm{n} / \mathrm{a}^{\mathrm{B}}$ | - | - |
| Stop-control | NB Left: A (8.2s) | 0.06 | $<10 \mathrm{~m}$ | NB Left: A (7.9s) | 0.02 | $<10 \mathrm{~m}$ |
|  | EB Lt-Rt: B (10.9s) | 0.02 | $<10 \mathrm{~m}$ | EB Lt-Rt: B (11.4s) | 0.15 | $<10 \mathrm{~m}$ |

\#9: Trunk 2 / Parcel F Residential Access

|  | AM Peak Hour |  | PM Peak Hour |  |  |  |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
|  | Approach: LOS <br> (Delay) | V/C | Queue $^{\mathrm{A}}$ | Approach: LOS <br> (Delay) | V/C | Queue $^{\mathrm{A}}$ |
|  | $\mathrm{n} / \mathrm{a}$ | - | - | $\mathrm{n} / \mathrm{a}$ | - | - |
| Background 2043 ${ }^{\mathrm{C}}$ | $\mathrm{n} / \mathrm{a}$ | - | - | $\mathrm{n} / \mathrm{a}$ | - | - |
| Total 2043 | SB Th-Rt: $\mathrm{n} / \mathrm{a}^{\mathrm{B}}$ | - | - | SB Th-Rt: $\mathrm{n} / \mathrm{a}^{\mathrm{B}}$ | - | - |
| Stop-control | NB Left: $\mathbf{A}(7.8 \mathrm{~s})$ | 0.02 | $<10 \mathrm{~m}$ | NB Left: $\mathbf{A}(7.9 \mathrm{~s})$ | 0.05 | $<10 \mathrm{~m}$ |
|  | EB Lt-Rt: B (11.0s) | 0.15 | $<10 \mathrm{~m}$ | EB Lt-Rt: B (11.0s) | 0.07 | $<10 \mathrm{~m}$ |

[^6]Table 16 -continued
\#10: Road A / Parcel D Commercial Access

|  | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {A }}$ | Approach: LOS (Delay) | V/C | Queue ${ }^{\text {A }}$ |
| Existing 2023 ${ }^{\text {c }}$ <br> No intersection | n/a | - | - | n/a | - | - |
| Background 2043 ${ }^{\text {c }}$ <br> No intersection | n/a | - | - | n/a | - | - |
| Total 2043 Stop-control | WB Th-Rt: $n / a^{B}$ <br> EB Left: A (8.0s) <br> SB Lt-Rt: C (20.0s) | $\begin{gathered} - \\ 0.09 \\ 0.49 \end{gathered}$ | $\begin{gathered} <10 \mathrm{~m} \\ 20 \mathrm{~m} \end{gathered}$ | WB Th-Rt: n/a ${ }^{B}$ <br> EB Left: A (8.2s) <br> SB Lt-Rt: C (15.5s) | $\begin{gathered} - \\ 0.06 \\ 0.36 \end{gathered}$ | $\begin{gathered} <10 \mathrm{~m} \\ 15 \mathrm{~m} \end{gathered}$ |

A - Queue represents the calculated vehicle queue length in metres occurring 95\% of the time ( $95^{\text {th }}$ percentile).
B - HCM methodology assumes no delay for this first order intersection movement. No results calculated.
$C$ - Intersection does not exist under this scenario.

The results contained in Table 16 suggest that all future traffic movements at the study area intersections are forecast to operate with good levels of service, delay times, volume-to-capacity ratios along with little to no queue build-up during the peak travel times. However, in order to achieve acceptable intersection performance measures there will be a need for new roadway infrastructure upgrades, including:

1. Trunk 2 / Wickwire South Street: Under our assumed 2043 Total traffic scenario, this intersection will require traffic signals and a northbound left turn lane.
2. Trunk 2 / Wickwire North Street: Under our assumed 2043 Total traffic scenario, this fourleg intersection can function adequately with stop-control, and auxiliary left turn lanes in both the north and southbound direction.
3. Trunk 2 / New Road A: This new three-leg intersection can function with stop-control under a full-build-out scenario. The warrant for a new northbound left turn auxiliary lane is met at this location.

The future lane configuration and traffic control upgrades are illustrated in Figure 12.

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Figure 12: Recommended Future Lane Configuration - $\mathbf{2 0 4 3}$ Horizon


## 7. INTERNAL STREET NETWORK

This chapter provides a summary of the proposed new street system and an assessment of the new connections to Trunk 2.

### 7.1 New Connections to Trunk 2

### 7.1.1 Overview

GRIFFIN completed a driver visibility review at the three new connections proposed as part of the FH Development neighbourhood. These connections include the Road A intersection, the Parcel B access, and the Parcel F access.

At this early stage of the planning approval process, NSDPW requires proponents to apply their Sight Distance Policy Procedure (PR5000) to determine if a proposed new access is provided in a suitable location. The procedure is applicable to drivers traveling on the major road approaching the new intersection/access and ensures there is sufficient distance for them to identify a hazard and bring their vehicle to a stop. The minimum criterion for approaching vehicles is referred to as Stopping Sight Distance (SSD). The NSDPW Procedure generally follows guidelines contained in the Transportation Association of Canada's (TAC) Geometric Design Guide for Canadian Roads ${ }^{3}$ document using a driver eye height of 1.05 m , an object height of 0.60 m , as well as the observed $85^{\text {th }}$ percentile operating speeds.

GRIFFIN gathered vehicle operating speed data north of the Robert Scott Drive intersection, near the proposed connection for Road A. These data were gathered in November 2022. This location is situated in the vicinity of a speed limit transition zone from $60 \mathrm{~km} / \mathrm{h}$ to $80 \mathrm{~km} / \mathrm{h}$.

The calculated $85^{\text {th }}$ percentile vehicle operating speeds were determined to be $82 \mathrm{~km} / \mathrm{h}$. However, as this area continues to grow and become less rural and more suburban, it is expected that the MEH and NSDPW will extend the $60 \mathrm{~km} / \mathrm{h}$ speed zone further north along Trunk 2 - beyond the proposed development. We have assumed operating speeds in the vicinity of the proposed Road A intersection would be much less in the future and have used $60 \mathrm{~km} / \mathrm{h}$ for the visibility review discussed in the following Section.

### 7.1.2 Stopping Sight Distance Review

A summary of the field measured sight distances relative to the minimum requirements for a 60 $\mathrm{km} / \mathrm{h}$ operating speed is provided in Table 17.

[^7]Table 17: Summary of Stopping Sight Distance Measurements ( $60 \mathrm{~km} / \mathrm{h}$ )

| Measurement Location | Travel Direction | $\begin{gathered} \text { Available } \\ \text { SSD } \end{gathered}$ | TAC Required SSD |  | Does Available Exceed Required? |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Base ${ }^{\text {A }}$ | Slope Adjusted |  |
| 1. Proposed New Road A (at field access) | Northbound | 93 m | $\begin{gathered} 85 \mathrm{~m} \\ (60 \mathrm{~km} / \mathrm{h}) \end{gathered}$ | $80 \mathrm{~m}(+3 \%)^{\text {B }}$ | Yes |
|  | Southbound | 250 m |  | $85 \mathrm{~m}(0 \%)^{\text {B }}$ | Yes |
| 2. Proposed New Parcel B Access (270m south of $\mathrm{P} / \mathrm{L}$ ) | Northbound | 150m | $\begin{gathered} 85 \mathrm{~m} \\ (60 \mathrm{~km} / \mathrm{h}) \end{gathered}$ | $85 \mathrm{~m}(0 \%)^{\text {B }}$ | Yes |
|  | Southbound | 105 m |  | $85 \mathrm{~m}(0 \%)^{\text {B }}$ | Yes |
| 3. Proposed New Parcel F Access ( 50 m south of $\mathrm{P} / \mathrm{L}$ ) | Northbound | 115 m | $\begin{gathered} 85 \mathrm{~m} \\ (60 \mathrm{~km} / \mathrm{h}) \end{gathered}$ | $87 \mathrm{~m}(-3 \%)^{\text {B }}$ | Yes |
|  | Southbound | 160m |  | $87 \mathrm{~m}(-3 \%)^{\text {B }}$ | Yes |

A - 2017 TAC Chapter 2, Table 2.5.2
$B$ - An estimate of the actual slope along Trunk 2 on the approaches to the new access.

GRIFFIN concluded from the driver visibility review findings that the three proposed new connections to Trunk 2 can be placed in locations that offer sufficient stopping sight distance for a future $60 \mathrm{~km} / \mathrm{h}$ operating speed.

### 7.2 Accommodating Public Transit Service in the Future

It is understood that the MEH has plans to implement public transit service at some point in the future. This type of transportation service is essential for a growing community, once population and employment levels reach feasible levels. There is; however, a notable investment of time and resources for a Municipality to plan and implement such a service - activities that could include route planning, service thresholds, investments in a bus fleet, adequate maintenance and storage facilities, hiring personnel, and so forth. Given these conditions, it is expected that the introduction of transit service is likely to occur in the medium to long-term timeframe.

Planning for a public transit service; however, can begin now to ensure the future service can be implemented more efficiently. It would be prudent for the Municipality to make provisions for public transit bus service during the planning and design stages - particularly along collector streets - with in the new development areas in Lantz. This includes the FH Development proposed Mixed Use neighbourhood.

As the Municipality continues through the planning approval process, they should work with FH Developments to identify future potential bus route corridor(s) within the proposed development. These specific streets may require design adjustments to accommodate the larger transit vehicles. In addition, a successful transit system requires good connectivity with other travel modes - such as active transportation.

We should note that despite the future plans to implement public transit, GRIFFIN has not modified the vehicle trip generation rates applied to this study to account for any mode shift from
commuter vehicle travel to public transit travel. This provides a more conservative and worst-case set of results - particularly if transit service is not introduced until a long-term time frame.

### 7.3 Active Transportation Facilities

Planning and designing communities following Smart Growth guidelines and principles will help a Municipality reduce dependency on auto travel, and in turn, will encourage greater use of other modes such as public transit, walking, and cycling. A successful Smart Growth strategy relies on the ability of the plan to offer residents with multiple choices for their mode of travel when making trips. We discussed the potential for a future public transit service in this area of MEH in the previous Section, but there is more that can be implemented to help achieve these goals.

The MEH should give consideration to providing active transportation facilities throughout the growing area of Lantz. New neighbourhoods that are being planned should attempt to incorporate active transportation trails and multi-use pathways that offer convenient connectivity between neighbourhoods. Asphalt multi-use paths (MUP) could be implemented in the street boulevard area, in place of typical concrete sidewalks. An example of a MUP is contained in Figure 13.

Figure 13: Example of a Multi-Use Path Along a Street


Source: OTM Book 18: Cycling Facilities

These types of active transportation facilities offer a safe and comfortable area to travel regardless of age or ability. They also offer good connectivity between the active modes and public transit and should be considered along all new collector streets, as well as connecting schools, recreational centres and so forth.

## 8. TRUNK 2 CORRIDOR SENSITIVITY ANALYSIS

This chapter summarizes the analysis results of our long-term full build-out sensitivity analysis. The assessment only focuses on the capacity needs of the new intersections along Trunk 2.

### 8.1 Overview

Throughout the Province, the demand for residential housing units has increased in the last few years - beyond what was previously contemplated. Specific to our study area, there is now expected to be a notable increase in population and employment in the Lantz area over the next 20-40 years. Therefore, the NSDPW has concerns with the long-term functionality of the Trunk 2 corridor in Lantz. As such, the NSDPW has requested that an additional sensitivity assessment be completed to better understand the future Trunk 2 corridor capacity needs.

Establishing the vehicle demand for the sensitivity assessment was less focused on a specific planning horizon - which is the typical approach for transportation planning assessments - and more focused on a specific full build-out scenario. As identified through discussions with NSDPW, the assumed full build-out scenario assumed that both the Wickwire Development and FH Development's East Milford Development were completed. We have focused specifically on these two developments in the Lantz north area as they are anticipated to contribute to the majority of vehicle demand on Trunk 2, in the vicinity of the NSDPW's area of concern. The assumed development rates for the key development areas are summarized in Table 18.

Table 18: Assumed Future Full Build-Out Rates - Sensitivity Analysis (3,666 units)

| Development Name | Residential <br> (units) | Commercial <br> $\left(\mathbf{f t}^{2}\right)$ |
| :---: | :---: | :---: |
| Lantz North / Wickwire Station | 2,115 | $50,000 \mathrm{ft}^{\mathbf{2}}$ |
| FH Development East Milford | 1,551 | $47,000 \mathrm{ft}^{2}$ |
| TOTALS | $\mathbf{3 , 6 6 6} \mathbf{u n i t s}$ | $\mathbf{9 7 , 0 0 0} \mathrm{ft}^{\mathbf{2}}$ |

The analysis component to our sensitivity assessment was focused only on the new intersections along the Trunk 2 corridor in the vicinity of the Lantz North / Wickwire development. As such, we have only evaluated the Wickwire South Street, Wickwire North Street-Robert Scott Drive, and the new FH Development Road A intersections.

### 8.2 Peak Hour Traffic Volumes

The future full build-out peak hour traffic volumes utilized the same source documents as applied to our analysis of the 2043 Total development scenario, presented earlier in Section 6. The Wickwire Development site-generated traffic was referenced from the WSP 2019 TIS report (Figures 2 A and B ). The East Milford site-generated traffic volumes were referenced from Section

4 of this report. GRIFFIN then assembled the sensitivity analysis peak hour volumes and these are contained in Figure 14.

Figure 14: Future Trunk 2 Corridor Peak Hour Vehicle Demand - Sensitivity Analysis Scenario


### 8.3 Analysis Results

### 8.3.1 Signal Warrant Results

Following the same analysis methodology as presented earlier in Section 6.1, GRIFFIN calculated the need for traffic control upgrades at each of the three intersections - assuming the future peak hour vehicle demand contained in Figure 14. The traffic signal warrant results are presented in Table 19, along with detailed calculations provided in Appendix II.

Table 19: Summary of Traffic Signal Warrant Results - Sensitivity Analysis (3,666 units)

| Intersection No. \& Location | Sensitivity Analysis Results |  |
| :---: | :---: | :---: |
|  | Baseline 2023 | Future Full Build-Out |
| \#5: Trunk 2 / Wickwire South St | $\mathrm{n} / \mathrm{a}^{\mathrm{A}}$ | 415 points |
| \#6: Trunk 2 / Robert Scott-Wickwire North St | 3 points | 140 points $^{\mathrm{B}}$ |
| \#7: Trunk 2 / New Road A | $\mathrm{n} / \mathrm{a}^{\mathrm{A}}$ | 81 points |

A - Intersection does not exist under this development scenario.
$B$ - Assumes the existing three-leg intersection is converted to a four-leg intersection to accommodate the new west access connection.

Upgrades to either traffic signals or roundabouts are expected to be needed at both the Wickwire South Street intersection (415 points) and the Wickwire North Street intersection (140 points) under a future full build-out scenario. Since the majority of traffic flow is expected to move to/from the south along Trunk 2, the vehicle demand north of the future Wickwire Development are similar to the 2043 peak hour volumes contained in Figure 11. Therefore, the Trunk 2 / New Road A intersection is expected to operate with acceptable performance measures as a stopcontrol intersection (81 points).

### 8.3.2 Auxiliary Turn Lane Warrant Results

The auxiliary turn lane warrant results for the Road A unsignalized intersection are presented in Table 20, along with detailed calculations provided in Appendix III.

Table 20: Summary of Auxiliary Turn Lane Assessments- Sensitivity Analysis (3,666 units)

| Intersection No. \& Location | Sensitivity Analysis Results |  |  |
| :---: | :---: | :---: | :---: |
|  |  | Baseline 2023 | Future Full Build-Out |
| \#5: Trunk 2 / Wickwire South St | Left Turn Lane | $n / a^{A}$ | signalized $^{B}$ |
|  | Right Turn Lane | $n / a^{A}$ | signalized $^{B}$ |
| \#6: Trunk 2 / Robert Scott-Wickwire North St | Left Turn Lane | Warrant not met | signalized $^{B}$ |
|  | Right Turn Lane | Warrant not met | signalized $^{B}$ |
| \#7: Trunk 2 / New Road A | Left Turn Lane | $n / a^{A}$ | Warrant met |
|  | Right Turn Lane | $n / a^{A}$ | Warrant not met |

A - This intersection does not exist under this development scenario.
$B$ - Results provided only for scenarios with stop-control. Future Total scenario requires signalization, thus no results.

As identified in the previous section, only the new Road A intersection will be able to operate with stop-control. The warrant is met for a northbound auxiliary left turn lane at this location. The warrant is not met for the southbound right turn lane.

### 8.3.3 Intersection Performance Results

A summary of the operational performance at the three key intersections is summarized in Table 21.

Table 21: Intersection Operational Analysis Results - Sensitivity Analysis (3,666 units)

| \#5: Trunk 2 / Wickwire South St |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | AM Peak Hour |  | PM Peak Hour |  |  |  |
|  | Approach: LOS <br> (Delay) | V/C | Queue $^{\text {A }}$ | Approach: LOS <br> (Delay) | V/C | Queue $^{\text {A }}$ |
|  |  |  |  |  |  |  |
| Full Build-out | SB Entry: D (42.4s) | 0.92 | 120 m | SB Entry: D (50.0s) | 0.93 | 105 m |
| Sensitivity Analysis | NB Entry: C (24.4s) | 0.81 | 70 m | NB Entry: C (27.5s) | 0.96 | 210 m |
| Signalized | EB Entry: D (38.8s) | 0.95 | 130 m | EB Entry: B (15.7s) | 0.73 | 25 m |
| Trunk 2: 4-lanes |  |  |  |  |  |  |

\#6: Trunk 2 / Robert Scott Dr-Wickwire North St

|  | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :--- | :--- | :---: | :---: | :--- | :---: | :---: |
|  | Approach: LOS <br> (Delay) | V/C | Queue $^{\text {A }}$ | Approach: LOS <br> (Delay) | V/C | Queue $^{\text {A }}$ |
|  | SB Entry: B (19.3s) | 0.60 | 105 m | SB Entry: B (16.1s) | 0.51 | 80 m |
| Sensitivity Analysis | NB Entry: A (6.9s) | 0.32 | 40 m | NB Entry: B (14.2s) | 0.84 | 80 m |
| Signalized | EB Entry: B (17.0s) | 0.78 | 35 m | EB Entry: B (12.4s) | 0.63 | 20 m |
| Trunk 2: 2-lanes | WB Entry: C (25.8s) | 0.16 | 15 m | WB Entry: C (25.4s) | 0.09 | 10 m |

\#7: Trunk 2 / New Road A

|  | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :--- | :--- | :---: | :---: | :--- | :---: | :---: |
|  | Approach: LOS <br> (Delay) | V/C | Queue $^{\text {A }}$ | Approach: LOS <br> (Delay) | V/C | Queue $^{\text {A }}$ |
|  | SB Th-Rt: $\mathrm{n} / \mathrm{a}^{\mathrm{B}}$ | - | - | SB Th-Rt: $\mathrm{n} / \mathrm{a}^{\mathrm{B}}$ | - | - |
| Sensitivity Analysis | NB Left: A (8.4s) | 0.11 | $<10 \mathrm{~m}$ | NB Left: A (9.1s) | 0.22 | 10 m |
| Stop-control | EB Left: C (23.7s) | 0.37 | 15 m | EB Left: E (46.9s) | 0.49 | 20 m |
| Trunk 2: 2-lanes | EB Right: B (13.2s) | 0.40 | 15 m | EB Right: B (12.2s) | 0.25 | 10 m |

A - Queue represents the calculated vehicle queue length in metres occurring 95\% of the time (95 ${ }^{\text {th }}$ percentile).
$B$ - HCM methodology assumes no delay for this first order intersection movement. No results calculated.
$C$ - Intersection does not exist under this scenario.

### 8.4 Discussion of Long-Term Corridor Capacity Needs

Based on the findings of our long-term full build-out sensitivity analysis, we can expect the need for traffic signals at both Wickwire North and South intersections. In terms of roadway crosssection, there is a need to widen Trunk 2 south of the future Wickwire South Street intersection to four lanes (i.e. two travel lanes in each direction). North of this location, Trunk 2 can adequately function with the capacity offered by a two-lane cross-section (i.e. one travel lane in each direction). The expected lane configuration needs are generally shown in Figure 15.

It should be noted that this a long-term view of the corridor capacity needs - a timeframe that is likely to extend beyond the 2043 planning horizon selected for this study. However, these findings are important as they suggest that there will be a need for a significant investment to widen the Trunk 2 corridor in order to accommodate the expected long-term population and employment growth in Lantz. In conclusion, there appears to be multiple future transportation planning options for this area of the MEH:

- Widen Trunk 2 to four lanes to move vehicle demand between the new neighbourhoods in Lantz north and the new Lantz interchange,
- Begin planning for a new Highway 102 interchange in the east Milford / Milford area to help dissipate the concentration of vehicle demand to/from the south and avoid the need to widen Trunk 2, or
- Implement new land use policies, introduce public transit with an attractive level of service, and offer multiple travel mode options for future residents. These initiatives will help reduce some of the demand for auto travel, and are likely only able to defer the need for capacity upgrades.

Upon rationalizing these three candidate long-term solutions, GRIFIN recommends that the NSDPW begin the planning process for a new Highway 102 interchange. This work will help identify an appropriate location as well as assist in preserving the necessary right-of-way once the need for this facility is reached.

Figure 15: Trunk 2 Long-Term Corridor Lane Configuration


## 9. CONCLUSIONS AND RECOMMENDATIONS

This chapter summarizes the salient findings of the analysis and identifies any necessary changes to the transportation infrastructure.

### 9.1 Conclusions

The following conclusions were gleaned from this traffic impact assessment:

- The Proposed Development: The proponent has plans to develop the vacant PID \#45089802 property into a Mixed Use neighbourhood that will be comprised of up to 1,551 new residential units and about $47,000 \mathrm{ft}^{2}$ of supporting commercial space. Vehicle access to this development will be provided by several new connections to Trunk 2. It is understood that the MEH has future plans to offer public transit service and this development is being planned to accommodate this service once it is ready to be implemented. This will offer future residents of this neighbourhood, as well as other adjacent neighbourhoods, with travel mode options which may help reduce auto demand in the area.
- New Vehicle Traffic: The expected new vehicle traffic generated by the proposed Mixed Use development was calculated using ITE's latest trip rates contained in the Trip Generation Manual, $11^{\text {th }}$ Edition. The additional vehicle trips added to the road network include:
- AM Peak Hour: 1,328 vph (516 inbound, 812 outbound)
- PM Peak Hour: 1,380 vph (766 inbound, 614 outbound)
- Lantz Connector Road Corridor: The existing lane configuration and the existing capacity at each roundabout along this corridor is expected to sufficiently accommodate the forecast peak hour demand assumed to occur by the 2043 planning horizon. No future upgrades are expected at any of the existing roundabouts by 2043.
- New Connections along the Trunk 2 Corridor - 2043 Planning Horizon:
- GRIFFIN has assumed three new connections to Trunk 2 would be needed to accommodate the proposed Mixed Use development. They included one new intersection connection (Road A), as well as two new driveway connections (Parcel B and Parcel F). Our driver visibility review concluded there are suitable locations to make these connections assuming the future regulatory speed limit and operating speeds along Trunk 2 are reduced to $60 \mathrm{~km} / \mathrm{h}$ - a reduced speed environment is expected to occur as this area changes from rural to suburban.
- The three new Trunk 2 connections associated with the proposed development are expected to operate with acceptable performance measures with stopcontrol.
- The Wickwire South Street and North Street intersections are expected to also serve as connection options for the proposed development. Our examination of
these two future connections has identified the need for signalization at the Wickwire South Street intersection. The Wickwire North Street-Robert Scott Drive intersection is expected to function well with stop-control under the assumed 2043 Total peak hour traffic demand used in this study.
- Trunk 2 Corridor Beyond 2043: At the request of NSDPW, GRIFFIN completed a long-term full build-out sensitivity assessment in the vicinity of the new intersections along Trunk 2. It was determined that Trunk 2 is expected to require widening to a four-lane crosssection south of the Wickwire South Street intersection - in the absence of any other network capacity upgrades.

Overall, our traffic analysis results suggest the study area intersections can adequately accommodate the future Total 2043 peak hour volumes - assuming the transportation system upgrades noted above have been implemented. In addition, it can be concluded that the new sitegenerated vehicle trips associated with the proposed development result in volume increases along the Lantz Connector Road; however, this corridor will continue to offer sufficient capacity through the 2043 planning horizon.

### 9.2 Recommendations

The following recommendations were developed based on the findings flowing from this study:

1. Geometric Design Process: That the geometric design process for the new internal street system and its intersections with the existing public roads follow the most recent NSDPW and TAC geometric design guidelines. In addition, minimum required driver sight distances, corner sight triangles and corner clearances should be confirmed and maintained throughout the design and construction phases of the project. Prior to the start of any roadway or intersection design process, the proponent and their geometric design team will need to identify and confirm an appropriate design vehicle (eg. a snow removal truck or garbage truck).
2. Signs and Pavement Markings: That all new signage and pavement markings associated with any new intersections or roads be installed in accordance with the latest version of the Transportation Association of Canada's (TAC) Manual of Uniform Traffic Control Devices of Canada (MUTCDC).
3. New Internal Street System: That the geometric design team follow industry best practices when selecting an alignment for the new internal public streets and that the location of minor streets and commercial driveways along the new internal street system are placed in suitable locations. All municipal by-law requirements should be met including provisions for appropriate corner clearances to ensure new driveways serving the individual lots within the development are a sufficient distance away from intersections. The geometric design team should verify these requirements with the appropriate approving agency. Consideration of implementing active transportation facilities and design features such as curb extensions at intersections, accessibility features (eg. tactile warning pads at crosswalks), wider multi-use paths in place of a traditional sidewalks, and so forth will provide improved travel mode options for the future residents.
4. Implement the following Trunk 2 intersection/driveway upgrades as shown in Figure 12:

- Trunk 2 / Wickwire South Street: Signalization and a northbound left turn auxiliary lane likely needed prior to the 2043 planning horizon.
- Trunk 2 / Robert Scott-Wickwire North Street: Stop-control and north-south left turn auxiliary lanes, sufficient out to the 2043 planning horizon.
- Trunk 2 / New Road A: Stop-control and a northbound left turn auxiliary lane are sufficient out to the 2043 planning horizon. This new intersection should be located as close to the south property line as possible to maximize the driver visibility to/from the south along Trunk 2. The adjacent civic \#1520 driveway will need to be closed and relocated to connect to Road A to eliminate turning conflicts at the new intersection.
- New Driveways along Trunk 2: GRIFFIN recommends the following:
- Parcel F Driveway: One stop-controlled driveway with no auxiliary turn lanes. Providing only one vehicle access will be sufficient to accommodate the traffic generated by the assumed residential units contained within this parcel.
- Parcel B Driveway: One stop-controlled driveway with no auxiliary turn lanes. Providing only one vehicle access will be sufficient to accommodate the traffic generated by the assumed commercial space contained within this parcel.
- Parcel D Driveway: One stop-controlled driveway connecting to Road A, with as much corner clearance distance from Trunk 2 as possible. One driveway connection will be sufficient to serve the proposed highway commercial businesses assumed to be contained within this parcel.

5. Lower Trunk 2 Speed Limit: Shift the existing speed transition zone from Robert Scott Drive, northward, to beyond the Regional Service boundary (RSB). This will lower the regulatory speed limit along Trunk 2 to $60 \mathrm{~km} / \mathrm{h}$ through the study area. This is expected to be more consistent with the future suburban nature of this area.
6. Begin Long-Term Infrastructure Planning: As noted earlier in this report the Trunk 2 corridor is expected to adequately function with one through travel lane in each direction throughout the study area, out to the 2043 planning horizon. Beyond this timeframe; however, the full build-out of the known developments in this area will require widening of Trunk 2 to a four-lane cross-section south of the Wickwire South Street intersection. An alternative solution to extensive and intrusive widening is to provide a new Highway 102 interchange to better serve this growing area. It is recommended that NSDPW begin a long-term planning process to identify a suitable location for a new interchange facility.

## APPENDIX I

Observed Traffic Volumes

Turning Movement Count Report
Report Generated Using Turning Movement Count for Android by PortableStudies.com
Study Information

|  | Count Name | \% | $\begin{array}{lll} U=U \text { Turn } & L=\text { Left Turn } & T=T h r u \quad R=\text { Right Turn } \\ \text { P1 }=\text { Pedestrian Direction } 1 & P 2=\text { Pedestrian Direction 2 } \\ \text { Veh }=\text { Total Vehicles for Approach } \end{array}$ | Peak Hour Volume |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | LantzConn 102NBRamps AMPeak |  |  |  |  |
|  | Location |  |  | \% Vehs | \% HV's |
|  | LantzConn 102NBRamps AM Nov 17 22, Not Available |  |  | 93.3\% | 6.7\% |
|  | Performed By |  |  | \% Bank 3 | \% Bank 4 |
|  | Unknown |  |  | 0.0\% | 0.0\% |
|  | Date |  |  | Pedest | Volume |
|  | Thursday, November 17, 2022 |  |  |  |  |

Peak Hour Data

| $\begin{array}{\|l\|} \hline \begin{array}{l} \text { Time } \\ \text { Period } \end{array} \end{array}$ | Lantz Connector EB |  |  |  |  |  |  | Lantz Connector WB |  |  |  |  |  |  | Hwy 102 NB Off Ramp |  |  |  |  |  |  | Hwy 102 NB On Ramp |  |  |  |  |  |  | $\begin{gathered} \text { Total } \\ \text { Vehicles } \end{gathered}$ | $\begin{gathered} \text { Total } \\ \text { Pedestrians } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U | L | T | R | P1 | P2 | Veh | U | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh |  |  |
| 7:20 AM | 0 | 0 | 15 | 0 | 0 | 0 | 15 | 0 | 0 | 58 | 12 | 0 | 0 | 70 | 0 | 0 | 0 | 14 | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 99 | 0 |
| 7:35 AM | 0 | 1 | 19 | 0 | 0 | 0 | 20 | 0 | 0 | 45 | 20 | 0 | 0 | 65 | 0 | 0 | 1 | 24 | 0 | 0 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 110 | 0 |
| 7:50 AM | 0 | 0 | 11 | 0 | 0 | 0 | 11 | 0 | 0 | 39 | 18 | 0 | 0 | 57 | 0 | 0 | 1 | 13 | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 82 | 0 |
| 8:05 AM | 0 | 0 | 8 | 0 | 0 | 0 | 8 | 0 | 0 | 39 | 11 | 0 | 0 | 50 | 0 | 0 | 1 | 25 | 0 | 0 | 26 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 84 | 0 |

Vehicle Movement Summary

| $\begin{aligned} & \text { Movement } / \\ & \text { Details } \end{aligned}$ | Lantz Connector EB |  |  |  |  |  |  | Lantz Connector WB |  |  |  |  |  |  | Hwy 102 NB off Ramp |  |  |  |  |  |  | Hwy 102 NB On Ramp |  |  |  |  |  |  | Entire Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | u | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh | Vehicles | Pedestrians |
| Movement Volume | 0 | 1 | 53 | 0 | 0 | 0 | 54 | 0 | 0 | 181 | 61 | 0 | 0 | 242 | 0 | 0 | 3 | 76 | 0 | 0 | 79 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 375 | 0 |
| PHF | - | 0.25 | 0.70 | - | - | - | 0.68 | - | - | 0.78 | 0.76 | - | - | 0.86 | - | - | 0.75 | 0.76 | - | - | 0.76 | - | - | - | - | - | - | - | 0.85 | - |
| \% Vehs | 0.0\% | 100.0\% | 83.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 97.8\% | 85.2\% |  |  |  | 0.0\% | 0.0\% | 100.0\% | 96.1\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |  |  |
| \% HV's | 0.0\% | 0.0\% | 17.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 2.2\% | 14.8\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 3.9\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | Need a | m report? |
| \% Bank 3 | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | support@p | lestudies.com |
| \% Bank 4 | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |  |  |

Turning Movement Count Report
Report Generated Using Turning Movement Count for Android by PortableStudies.com
Study Information


Peak Hour Data

| $\begin{array}{\|l\|} \hline \begin{array}{l} \text { Time } \\ \text { Period } \end{array} \end{array}$ | Lantz Connector EB |  |  |  |  |  |  | Lantz Connector WB |  |  |  |  |  |  | Hwy 102 Off-Ramp |  |  |  |  |  |  | Hwy 102 On-Ramp |  |  |  |  |  |  | $\begin{gathered} \text { Total } \\ \text { Vehicles } \end{gathered}$ | $\begin{gathered} \text { Total } \\ \text { Pedestrians } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U | L | T | R | P1 | P2 | Veh | U | L | T | R | P1 | P2 | Veh | U | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh |  |  |
| 4:10 PM | 0 | 0 | 17 | 0 | 0 | 0 | 17 | 0 | 0 | 34 | 6 | 0 | 0 | 40 | 0 | 0 | 1 | 51 | 0 | 0 | 52 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 109 | 0 |
| 4:25 PM | 0 | 0 | 22 | 0 | 0 | 0 | 22 | 0 | 0 | 28 | 5 | 0 | 0 | 33 | 0 | 0 | 0 | 60 | 0 | 0 | 60 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 115 | 0 |
| 4:40 PM | 0 | 0 | 13 | 0 | 0 | 0 | 13 | 0 | 0 | 29 | 7 | 0 | 0 | 36 | 0 | 0 | 1 | 67 | 0 | 0 | 68 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 117 | 0 |
| 4:55 PM | 0 | 0 | 15 | 0 | 0 | 0 | 15 | 0 | 0 | 26 | 7 | 0 | 0 | 33 | 0 | 1 | 0 | 91 | 0 | 0 | 92 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 140 | 0 |

Vehicle Movement Summary

| $\begin{aligned} & \text { Movement } / \\ & \text { Details } \end{aligned}$ | Lantz Connector EB |  |  |  |  |  |  | Lantz Connector WB |  |  |  |  |  |  | Hwy 102 Off-Ramp |  |  |  |  |  |  | Hwy 102 On-Ramp |  |  |  |  |  |  | Entire Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | u | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh | Vehicles | Pedestrians |
| Movement Volume | 0 | 0 | 67 | 0 | 0 | 0 | 67 | 0 | 0 | 117 | 25 | 0 | 0 | 142 | 0 | 1 | 2 | 269 | 0 | 0 | 272 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 481 | 0 |
| PHF | - | - | 0.76 | - | - | - | 0.76 | - | - | 0.86 | 0.89 | - | - | 0.89 | - | 0.25 | 0.50 | 0.74 | - | - | 0.74 | - | - | - | - | - | - | - | 0.86 | - |
| \% Vehs | 0.0\% | 0.0\% | 77.6\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 95.7\% | 92.0\% |  |  |  | 0.0\% | 0.0\% | 100.0\% | 98.5\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |  |  |
| \% HV's | 0.0\% | 0.0\% | 22.4\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 4.3\% | 8.0\% |  |  |  | 0.0\% | 100.0\% | 0.0\% | 1.5\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | Need a | m report? |
| \% Bank 3 | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | support@p | lestudies.com |
| \% Bank 4 | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |  |  |

Turning Movement Count Report
Report Generated Using Turning Movement Count for Android by PortableStudies.com
Study Information


Peak Hour Data

| $\begin{aligned} & \text { Time } \\ & \text { Period } \end{aligned}$ | Lantz Connector EB |  |  |  |  |  |  | Shaw Dr WB |  |  |  |  |  |  | Tk 2 NB |  |  |  |  |  |  | Tk 2 SB |  |  |  |  |  |  | Total Vehicles | $\begin{gathered} \text { Total } \\ \text { Pedestrians } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | u | L | T | R | P1 | P2 | Veh | U | L | T | R | P1 | P2 | Veh | U | L | T | R | P1 | P2 | Veh | U | L | T | R | P1 | P2 | Veh |  |  |
| 7:10 AM | 0 | 16 | 2 | 9 | 0 | 0 | 27 | 0 | 1 | 1 | 0 | 0 | 0 | 2 | 0 | 6 | 19 | 1 | 0 | 0 | 26 | 0 | 1 | 39 | 59 | 0 | 0 | 99 | 154 | 0 |
| 7:25 AM | 0 | 13 | 3 | 23 | 0 | 0 | 39 | 0 | 1 | 3 | 0 | 0 | 0 | 4 | 0 | 9 | 14 | 2 | 0 | 0 | 25 | 0 | 0 | 56 | 57 | 0 | 0 | 113 | 181 | 0 |
| 7:40 AM | 0 | 15 | 5 | 18 | 0 | 0 | 38 | 0 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 27 | 43 | 1 | 0 | 0 | 71 | 0 | 2 | 68 | 41 | 0 | 0 | 111 | 222 | 0 |
| 7:55 AM | 0 | 11 | 7 | 11 | 0 | 0 | 29 | 0 | 0 | 2 | 1 | 0 | 0 | 3 | 0 | 8 | 45 | 0 | 0 | 0 | 53 | 0 | 0 | 35 | 45 | 0 | 0 | 80 | 165 | 0 |

Vehicle Movement Summary

| Movement / Details | Lantz Connector EB |  |  |  |  |  |  | Shaw Dr WB |  |  |  |  |  |  | Tk 2 NB |  |  |  |  |  |  | Tk 2 SB |  |  |  |  |  |  | Entire Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | u | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh | Vehicles | Pedestrians |
| Movement Volume | 0 | 55 | 17 | 61 | 0 | 0 | 133 | 0 | 2 | 7 | 2 | 0 | 0 | 11 | 0 | 50 | 121 | 4 | 0 | 0 | 175 | 0 | 3 | 198 | 202 | 0 | 0 | 403 | 722 | 0 |
| PHF | - | 0.86 | 0.61 | 0.66 | - | - | 0.85 | - | 0.50 | 0.58 | 0.50 | - | - | 0.69 | - | 0.46 | 0.67 | 0.50 | - | - | 0.62 | - | 0.38 | 0.73 | 0.86 | - | - | 0.89 | 0.81 | - |
| \% Vehs | 0.0\% | 90.9\% | 88.2\% | 85.2\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 100.0\% |  |  |  | 0.0\% | 90.0\% | 88.4\% | 100.0\% |  |  |  | 0.0\% | 100.0\% | 92.4\% | 98.5\% |  |  |  |  |  |
| \% HV's | 0.0\% | 9.1\% | 11.8\% | 14.8\% |  |  |  | 0.0\% | 100.0\% | 100.0\% | 0.0\% |  |  |  | 0.0\% | 10.0\% | 11.6\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 7.6\% | 1.5\% |  |  |  | Need a c | m report? |
| \% Bank 3 | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | suppor@po | lestudies.com |
| \% Bank 4 | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |  |  |

Turning Movement Count Report
Report Generated Using Turning Movement Count for Android by PortableStudies.com
Study Information


Peak Hour Data

| $\left\lvert\, \begin{aligned} & \text { Time } \\ & \text { Period } \end{aligned}\right.$ | Lantz Connector EB |  |  |  |  |  |  | Shaw Dr WB |  |  |  |  |  |  | Tk 2 NB |  |  |  |  |  |  | Tk 2 SB |  |  |  |  |  |  | TotalVehicles | $\begin{gathered} \text { Total } \\ \text { Pedestrians } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | u | L | T | R | P1 | P2 | Veh | U | L | T | R | P1 | P2 | Veh | U | L | T | R | P1 | P2 | Veh | U | L | T | R | P1 | P2 | Veh |  |  |
| 4:05 PM | 0 | 60 | 0 | 16 | 0 | 0 | 76 | 0 | 1 | 5 | 4 | 0 | 0 | 10 | 0 | 3 | 50 | 0 | 0 | 0 | 53 | 0 | 0 | 62 | 20 | 0 | 0 | 82 | 221 | 0 |
| 4:20 PM | 0 | 60 | 2 | 25 | 0 | 0 | 87 | 0 | 2 | 4 | 1 | 0 | 0 | 7 | 0 | 8 | 49 | 0 | 0 | 0 | 57 | 0 | 0 | 55 | 17 | 0 | 0 | 72 | 223 | 0 |
| 4:35 PM | 0 | 70 | 0 | 20 | 0 | 0 | 90 | 0 | 2 | 3 | 0 | 0 | 0 | 5 | 0 | 9 | 55 | 2 | 0 | 0 | 66 | 0 | 1 | 47 | 28 | 0 | 0 | 76 | 237 | 0 |
| 4:50 PM | 0 | 69 | 1 | 20 | 0 | 0 | 90 | 0 | 0 | 1 | 1 | 0 | 0 | 2 | 0 | 20 | 63 | 0 | 0 | 0 | 83 | 0 | 0 | 35 | 23 | 0 | 0 | 58 | 233 | 0 |

Vehicle Movement Summary

| $\begin{aligned} & \text { Movement / } \\ & \text { notailc } \end{aligned}$Details | Lantz Connector EB |  |  |  |  |  |  | Shaw Dr WB |  |  |  |  |  |  | Tk 2 NB |  |  |  |  |  |  | Tk 2 SB |  |  |  |  |  |  | Entire Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | u | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh | Vehicles | Pedestrians |
| Movement Volume | 0 | 259 | 3 | 81 | 0 | 0 | 343 | 0 | 5 | 13 | 6 | 0 | 0 | 24 | 0 | 40 | 217 | 2 | 0 | 0 | 259 | 0 | 1 | 199 | 88 | 0 | 0 | 288 | 914 | 0 |
| PHF | - | 0.93 | 0.38 | 0.81 | - | - | 0.95 | - | 0.63 | 0.65 | 0.38 | - | - | 0.60 | - | 0.50 | 0.86 | 0.25 | - | - | 0.78 | - | 0.25 | 0.80 | 0.79 | - | - | 0.88 | 0.96 | - |
| \% Vehs | 0.0\% | 96.5\% | 100.0\% | 87.7\% |  |  |  | 0.0\% | 80.0\% | 84.6\% | 66.7\% |  |  |  | 0.0\% | 82.5\% | 98.2\% | 50.0\% |  |  |  | 0.0\% | 100.0\% | 95.5\% | 94.3\% |  |  |  |  |  |
| \% HV's | 0.0\% | 3.5\% | 0.0\% | 12.3\% |  |  |  | 0.0\% | 20.0\% | 15.4\% | 33.3\% |  |  |  | 0.0\% | 17.5\% | 1.8\% | 50.0\% |  |  |  | 0.0\% | 0.0\% | 4.5\% | 5.7\% |  |  |  | Need a c | m report? |
| \% Bank 3 | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | suppor@po | lestudies.com |
| \% Bank 4 | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |  |  |

Turning Movement Count Report
Report Generated Using Turning Movement Count for Android by PortableStudies.com
Study Information


Peak Hour Data

| $\begin{array}{\|l\|} \text { Time } \\ \text { Period } \end{array}$ |  |  |  |  |  |  |  | Robert Scott |  |  |  |  |  |  | Tk 2 NB |  |  |  |  |  |  | Tk 2 SB |  |  |  |  |  |  | $\begin{gathered} \text { Total } \\ \text { Vehicles } \end{gathered}$ | $\begin{gathered} \text { Total } \\ \text { Pedestrians } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | u | L | T | R | P1 | P2 | Veh | U | L | T | R | P1 | P2 | Veh | U | L | T | R | P1 | P2 | Veh | U | L | T | R | P1 | P2 | Veh |  |  |
| 4:25 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 35 | 7 | 0 | 0 | 42 | 0 | 1 | 19 | 0 | 0 | 0 | 20 | 64 | 0 |
| 4:40 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 1 | 0 | 0 | 6 | 0 | 0 | 32 | 8 | 0 | 0 | 40 | 0 | 0 | 26 | 0 | 0 | 0 | 26 | 72 | 0 |
| 4:55 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 4 | 0 | 0 | 30 | 4 | 0 | 0 | 34 | 0 | 1 | 26 | 0 | 0 | 0 | 27 | 65 | 0 |
| 5:10 PM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 3 | 0 | 0 | 50 | 5 | 0 | 0 | 55 | 0 | 0 | 27 | 0 | 0 | 0 | 27 | 85 | 0 |

Vehicle Movement Summary

| $\begin{aligned} & \text { Movement / } \\ & \text { notailc } \end{aligned}$Details |  |  |  |  |  |  |  | Robert Scott |  |  |  |  |  |  | Tk 2 NB |  |  |  |  |  |  | Tk 2 SB |  |  |  |  |  |  | Entire Intersection |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | u | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh | u | L | T | R | P1 | P2 | Veh | Vehicles | Pedestrians |
| Movement Volume | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 4 | 0 | 0 | 15 | 0 | 0 | 147 | 24 | 0 | 0 | 171 | 0 | 2 | 98 | 0 | 0 | 0 | 100 | 286 | 0 |
| PHF | - | - | - | - | - | - | - | - | 0.55 | - | 0.50 | - | - | 0.63 | - | - | 0.74 | 0.75 | - | - | 0.78 | - | 0.50 | 0.91 | - | - | - | 0.93 | 0.84 | - |
| \% Vehs | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 100.0\% | 0.0\% | 100.0\% |  |  |  | 0.0\% | 0.0\% | 98.0\% | 95.8\% |  |  |  | 0.0\% | 100.0\% | 94.9\% | 0.0\% |  |  |  |  |  |
| \% HV's | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 2.0\% | 4.2\% |  |  |  | 0.0\% | 0.0\% | 5.1\% | 0.0\% |  |  |  | Need a c | m report? |
| \% Bank 3 | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | suppor@po | lestudies.com |
| \% Bank 4 | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |  |  |

## APPENDIX II

## TAC Traffic Signal Warrant Results



| Road Authority: | NSDPW |
| ---: | :---: |
| City: | Mun. of East Hants |
| Analysis Date: | 2023 Apr 14, Fri |
| Count Date: | 2022 Nov 14, Mon |
| Date Entry Format: | (yyyy-mm-dd) |
|  |  |


| Lane Configuration |  | V - x | ち \% \# |  | $\begin{aligned} & \leftrightarrows \\ & \stackrel{\rightharpoonup}{\rightleftarrows} \\ & \stackrel{\rightharpoonup}{ \pm} \\ & \underset{F}{2} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\sim} \\ & \stackrel{y}{*} \\ & \stackrel{F}{2} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\widetilde{v}} \\ & \stackrel{\rightharpoonup}{v} \\ & \hline \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Trunk 2 | NB | 1 |  | 1 |  |  |  | 2,000 | 1 |
| Trunk 2 | SB |  |  |  |  | 1 |  | 2,000 | 1 |
| Wickwire South Street | WB |  |  |  |  |  |  |  |  |
| Wickwire South Street | EB |  |  |  | 1 |  |  |  |  |
| Are the Wickwire South Street EB right turns significantly impeded by through movements? (y/n) |  |  |  |  |  |  | n |  |  |
|  |  |  |  |  |  |  | n |  |  |


| Demographics |  |  |
| :--- | :---: | :---: |
| Elem. School/Mobility Challenged | $(\mathrm{y} / \mathrm{n})$ | n |
| Senior's Complex | $(\mathrm{y} / \mathrm{n})$ | n |
| Pathway to School | $(\mathrm{y} / \mathrm{n})$ | n |
| Metro Area Population | $(\#)$ | 20,000 |
| Central Business District | $(\mathrm{y} / \mathrm{n})$ | n |


| Other input |  | $\begin{gathered} \text { Speed } \\ (\mathrm{Km} / \mathrm{h}) \end{gathered}$ | Truck \% | $\begin{gathered} \begin{array}{c} \text { Bus Rt } \\ (\mathrm{y} / \mathrm{n}) \end{array} \\ \hline \end{gathered}$ | Median (m) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Trunk 2 | NS | 60 | 5.0\% | n | 0.0 |  |  |  |  |  |  |  |  |  |  |  |
| Wickwire South Street | EW |  | 5.0\% | n |  |  |  |  |  |  |  |  |  |  |  |  |
| Set Peak Hours |  |  |  |  |  |  |  |  |  |  |  |  | Ped1 | Ped2 | Ped3 | Ped4 |
| Traffic Input |  | NB |  |  | SB |  |  | WB |  |  | EB |  | NS | NS | EW | EW |
|  | LT | Th | RT | LT | Th | RT | LT | Th | RT | LT | Th | RT | w Side | E Side | N Side | S Side |
| 7:00-8:00 | 43 | 118 | 0 | 0 | 221 | 3 | 0 | 0 | 0 | 8 | 0 | 132 | 5 | 5 | 5 | 5 |
| 8:00-9:00 | 57 | 156 | 0 | 0 | 293 | 4 | 0 | 0 | 0 | 10 | 0 | 175 | 5 | 5 | 5 | 5 |
| 12:00-13:00 | 133 | 218 | 0 | 0 | 138 | 8 | 0 | 0 | 0 | 8 | 0 | 77 | 5 | 5 | 5 | 5 |
| 13:00-14:00 | 143 | 234 | 0 | 0 | 149 | 9 | 0 | 0 | 0 | 9 | 0 | 83 | 5 | 5 | 5 | 5 |
| 16:00-17:00 | 191 | 312 | 0 | 0 | 198 | 12 | 0 | 0 | 0 | 12 | 0 | 111 | 5 | 5 | 5 | 5 |
| 17:00-18:00 | 179 | 293 | 0 | 0 | 186 | 11 | 0 | 0 | 0 | 11 | 0 | 104 | 5 | 5 | 5 | 5 |
| Total (6-hour peak) | 746 | 1,331 | 0 | 0 | 1,185 | 47 | 0 | 0 | 0 | 58 | 0 | 682 | 30 | 30 | 30 | 30 |
| Average (6-hour peak) | 124 | 222 | 0 | 0 | 198 | 8 | 0 | 0 | 0 | 10 | 0 | 114 | 5 | 5 | 5 | 5 |



Traffic Signal Warrant Spreadsheet - v3H © 2007 Transportation Association of Canada


| Lane Configuration |  | E c x | $$ | 宕 |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\alpha} \\ & \approx \\ & \stackrel{\#}{F} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{v} \\ & \frac{\rightharpoonup}{v} \\ & \text { n } \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Trunk 2 | NB | 1 |  | 1 |  |  |  | 2,000 | 1 |
| Trunk 2 | SB |  |  |  |  | 1 |  | 2,000 | 1 |
| Wickwire South Street | WB |  |  |  |  |  |  |  |  |
| Wickwire South Street | EB |  |  |  | 1 |  |  |  |  |
| Are the Wickwire South Street EB right turns significantly impeded by through movements? (y/n) |  |  |  |  |  |  | n |  |  |
|  |  |  |  |  |  |  | n |  |  |


| Other input |  | $\begin{gathered} \text { Speed } \\ (\mathrm{Km} / \mathrm{h}) \end{gathered}$ | Truck \% | Bus Rt ( $\mathrm{y} / \mathrm{n}$ ) | Median (m) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Trunk 2 | NS | 60 | 5.0\% | n | 0.0 |  |  |  |  |  |  |  |  |  |  |  |
| Wickwire South Street | EW |  | 5.0\% | n |  |  |  |  |  |  |  |  |  |  |  |  |
| Set Peak Hours |  |  |  |  |  |  |  |  |  |  |  |  | Ped1 | Ped2 | Ped3 | Ped4 |
| Traffic Input |  | NB |  |  | SB |  |  | WB |  |  | EB |  | NS | NS | EW | EW |
|  | LT | Th | RT | LT | Th | RT | LT | Th | RT | LT | Th | RT | W Side | E Side | N Side | S Side |
| 7:00-8:00 | 51 | 261 | 0 | 0 | 572 | 22 | 0 | 0 | 0 | 48 | 0 | 155 | 5 | 5 | 5 | 5 |
| 8:00-9:00 | 67 | 346 | 0 | 0 | 758 | 29 | 0 | 0 | 0 | 63 | 0 | 205 | 5 | 5 | 5 | 5 |
| 12:00-13:00 | 157 | 522 | 0 | 0 | 354 | 45 | 0 | 0 | 0 | 36 | 0 | 91 | 5 | 5 | 5 | 5 |
| 13:00-14:00 | 169 | 562 | 0 | 0 | 381 | 49 | 0 | 0 | 0 | 38 | 0 | 98 | 5 | 5 | 5 | 5 |
| 16:00-17:00 | 225 | 749 | 0 | 0 | 508 | 65 | 0 | 0 | 0 | 51 | 0 | 131 | 5 | 5 | 5 | 5 |
| 17:00-18:00 | 211 | 702 | 0 | 0 | 476 | 61 | 0 | 0 | 0 | 48 | 0 | 123 | 5 | 5 | 5 | 5 |
| Total (6-hour peak) | 880 | 3,142 | 0 | 0 | 3,049 | 271 | 0 | 0 | 0 | 284 | 0 | 803 | 30 | 30 | 30 | 30 |
| Average (6-hour peak) | 147 | 524 | 0 | 0 | 508 | 45 | 0 | 0 | 0 | 47 | 0 | 134 | 5 | 5 | 5 | 5 |



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| Date Entry Format: | (yyyy-mm-dd) |
|  |  |



| Demographics |  |  |
| :--- | :---: | :---: |
| Elem. School/Mobility Challenged | $(\mathrm{y} / \mathrm{n})$ | n |
| Senior's Complex | $(\mathrm{y} / \mathrm{n})$ | n |
| Pathway to School | $(\mathrm{y} / \mathrm{n})$ | n |
| Metro Area Population | $(\#)$ | 20,000 |
| Central Business District | $(\mathrm{y} / \mathrm{n})$ | n |


| Other input |  | $\begin{gathered} \text { Speed } \\ (\mathrm{Km} / \mathrm{h}) \end{gathered}$ | Truck \% | Bus Rt ( $\mathrm{y} / \mathrm{n}$ ) | Median (m) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Trunk 2 | NS | 60 | 5.0\% | n | 0.0 |  |  |  |  |  |  |  |  |  |  |  |
| Wickwire South Street | EW |  | 5.0\% | n |  |  |  |  |  |  |  |  |  |  |  |  |
| Set Peak Hours |  |  |  |  |  |  |  |  |  |  |  |  | Ped1 | Ped2 | Ped3 | Ped4 |
| Traffic Input |  | NB |  |  | SB |  |  | WB |  |  | EB |  | NS | NS | EW | EW |
|  | LT | Th | RT | LT | Th | RT | LT | Th | RT | LT | Th | RT | W Side | E Side | N Side | S Side |
| 7:00-8:00 | 157 | 306 | 0 | 0 | 699 | 29 | 0 | 0 | 0 | 65 | 0 | 456 | 5 | 5 | 5 | 5 |
| 8:00-9:00 | 208 | 406 | 0 | 0 | 926 | 38 | 0 | 0 | 0 | 86 | 0 | 605 | 5 | 5 | 5 | 5 |
| 12:00-13:00 | 462 | 638 | 0 | 0 | 426 | 64 | 0 | 0 | 0 | 56 | 0 | 274 | 5 | 5 | 5 | 5 |
| 13:00-14:00 | 497 | 686 | 0 | 0 | 458 | 69 | 0 | 0 | 0 | 61 | 0 | 295 | 5 | 5 | 5 | 5 |
| 16:00-17:00 | 662 | 915 | 0 | 0 | 611 | 92 | 0 | 0 | 0 | 81 | 0 | 393 | 5 | 5 | 5 | 5 |
| 17:00-18:00 | 621 | 858 | 0 | 0 | 573 | 86 | 0 | 0 | 0 | 76 | 0 | 369 | 5 | 5 | 5 | 5 |
| Total (6-hour peak) | 2,607 | 3,809 | 0 | 0 | 3,693 | 378 | 0 | 0 | 0 | 425 | 0 | 2,392 | 30 | 30 | 30 | 30 |
| Average (6-hour peak) | 435 | 635 | 0 | 0 | 616 | 63 | 0 | 0 | 0 | 71 | 0 | 399 | 5 | 5 | 5 | 5 |



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NSDPW - Traffic Signal Warrant Analysis


| Lane Configuration |  | E c x | ち \% E | 哭 |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\approx} \\ & \approx \\ & \stackrel{\#}{F} \end{aligned}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Trunk 2 | NB |  |  |  |  | 1 |  | 2,000 | 1 |
| Trunk 2 | SB |  | 1 |  |  |  |  | 2,000 | 1 |
| Robert Scott Dr | WB |  |  |  | 1 |  |  |  |  |
| Robert Scott Dr | EB |  |  |  |  |  |  |  |  |
| Are the Robert Scott Dr WB right turns significantly impeded by through movements? (y/n) |  |  |  |  |  |  | n |  |  |
|  |  |  |  |  |  |  | n |  |  |


| Road Authority: | NSDPW |
| ---: | :---: |
| City: | Mun. of East Hants |
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|  |  |




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| Road Authority: | NSDPW |
| ---: | :---: |
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NSDPW - Traffic Signal Warrant Analysis


| Road Authority: | NSDPW |
| ---: | :---: |
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|  |  |


| Lane Configuration |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{*} \\ & \otimes \\ & \stackrel{ت}{F} \end{aligned}$ |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{*} \\ & \approx \\ & \underset{\sharp}{\#} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Trunk 2 | NB | 1 |  |  |  | 1 |  | 980 | , |  |  |  | Demogra |  |  |  |
| Trunk 2 | SB | 1 |  |  |  | 1 |  | 2,000 | 1 |  |  |  | Elem. Sch | 1/Mobili | hallenged | (y/n) |
| Robert Scott Dr | WB |  |  |  | 1 |  |  |  |  |  |  |  | Senior's C | pplex |  | (y/n) |
| Robert Scott Dr | EB |  |  |  | 1 |  |  |  |  |  |  |  | Pathway to | School |  | (y/n) |
| Are the Robert Scott Dr WB right turns significantly impeded by through movements? (y/n) Are the Robert Scott Dr EB right turns significantly impeded by through movements? ( $\mathrm{y} / \mathrm{n}$ ) |  |  |  |  |  |  | n |  |  |  |  |  | Metro Ar | Populatio |  | (\#) |
|  |  |  |  |  |  |  | n |  |  |  |  |  | Central Business District |  |  | (y/n) |
| Other input |  | Speed (Km/h) | $\begin{gathered} \hline \text { Truck } \\ \% \end{gathered}$ | Bus Rt ( $\mathrm{y} / \mathrm{n}$ ) | Median (m) |  |  |  |  |  |  |  |  |  |  |  |
| Trunk 2 | NS | 60 | 5.0\% | n | 0.0 |  |  |  |  |  |  |  |  |  |  |  |
| Robert Scott Dr | EW |  | 5.0\% | n |  |  |  |  |  |  |  |  |  |  |  |  |
| Set Peak Hours |  |  |  |  |  |  |  |  |  |  |  |  | Ped1 | Ped2 | Ped3 | Ped4 |
| Traffic Input |  | NB |  |  | SB |  |  | WB |  |  | EB |  | NS | NS | EW | EW |
|  | LT | Th | RT | LT | Th | RT | LT | Th | RT | LT | Th | RT | W Side | E Side | N Side | S Side |
| 7:00-8:00 | 104 | 238 | 9 | 2 | 366 | 10 | 21 | 1 | 4 | 26 | 1 | 312 | 5 | 5 | 5 | 5 |
| 8:00-9:00 | 138 | 315 | 12 | 2 | 485 | 13 | 28 | 1 | 5 | 34 | 1 | 413 | 5 | 5 | 5 | 5 |
| 12:00-13:00 | 310 | 333 | 20 | 1 | 273 | 27 | 8 | 1 | 3 | 15 | 1 | 185 | 5 | 5 | 5 | 5 |
| 13:00-14:00 | 334 | 359 | 21 | 2 | 293 | 29 | 9 | 1 | 4 | 16 | 1 | 199 | 5 | 5 | 5 | 5 |
| 16:00-17:00 | 445 | 478 | 28 | 2 | 391 | 39 | 12 | 1 | 5 | 21 | 1 | 265 | 5 | 5 | 5 | 5 |
| 17:00-18:00 | 417 | 448 | 26 | 2 | 367 | 37 | 11 | 1 | 5 | 20 | 1 | 249 | 5 | 5 | 5 | 5 |
| Total (6-hour peak) | 1,748 | 2,171 | 116 | 11 | 2,175 | 155 | 89 | 6 | 26 | 132 | 6 | 1,623 | 30 | 30 | 30 | 30 |
| Average (6-hour peak) | 291 | 362 | 19 | 2 | 363 | 26 | 15 | 1 | 4 | 22 | 1 | 271 | 5 | 5 | 5 | 5 |



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| Lane Configuration |  | $\begin{aligned} & \leftrightarrows \\ & \vdots \\ & \stackrel{x}{y} \end{aligned}$ |  |  |  |  | $\begin{aligned} & \underset{\sim}{v} \\ & \stackrel{\rightharpoonup}{v} \\ & \hline \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Trunk 2 | NB | 1 |  | 1 |  |  |  | 1,400 | 1 |
| Trunk 2 | SB |  |  |  |  | 1 |  | 2,000 | 1 |
| New Road A | WB |  |  |  |  |  |  |  |  |
| New Road A | EB |  |  |  | 1 |  |  |  |  |
| Are the New Road A EB right turns significantly impeded by through movements? (y/n) |  |  |  |  |  |  | n |  |  |
|  |  |  |  |  |  |  | n |  |  |




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| Comments | Direction (EW or NS) | NS |
| :---: | :---: | :---: |
|  | Direction (EW or NS) | EW |
|  | 2043 Volumes Total Scenario Sensitivity Dev. Scena |  |


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|  |  |


| Lane Configuration |  | 言 |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\rightleftarrows} \\ & \stackrel{y}{*} \\ & \stackrel{\sim}{4} \\ & \hline \end{aligned}$ |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\widetilde{v}} \\ & \stackrel{\rightharpoonup}{x} \\ & \hline \end{aligned}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Trunk 2 | NB | 1 |  | 1 |  |  |  | 415 | 1 |
| Trunk 2 | SB |  |  |  |  | 1 |  | 2,000 | 1 |
| New Road A | WB |  |  |  |  |  |  |  |  |
| New Road A | EB |  |  |  | 1 |  |  |  |  |
| Are the New Road A EB right turns significantly impeded by through movements? (y/n) |  |  |  |  |  |  | n |  |  |
|  |  |  |  |  |  |  | n |  |  |


| Demographics |  |  |
| :--- | :---: | :---: |
| Elem. School/Mobility Challenged | $(\mathrm{y} / \mathrm{n})$ | n |
| Senior's Complex | $(\mathrm{y} / \mathrm{n})$ | n |
| Pathway to School | $(\mathrm{y} / \mathrm{n})$ | n |
| Metro Area Population | $(\#)$ | 20,000 |
| Central Business District | $(\mathrm{y} / \mathrm{n})$ | n |




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| Other input |  | $\begin{gathered} \hline \text { Speed } \\ (\mathrm{Km} / \mathrm{h}) \\ \hline \end{gathered}$ | Truck <br> \% | $\begin{gathered} \begin{array}{c} \text { Bus Rt } \\ (\mathrm{y} / \mathrm{n}) \end{array} \\ \hline \end{gathered}$ | Median <br> (m) |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Trunk 2 | NS | 60 | 5.0\% | n | 0.0 |  |  |  |  |  |  |  |  |  |  |  |
| Parcel B Comm Dwy | EW |  | 5.0\% | n |  |  |  |  |  |  |  |  |  |  |  |  |
| Set Peak Hours |  |  |  |  |  |  |  |  |  |  |  |  | Ped1 | Ped2 | Ped3 | Ped4 |
| Traffic Input |  | NB |  |  | SB |  |  | WB |  |  | EB |  | NS | NS | EW | EW |
|  | LT | Th | RT | LT | Th | RT | LT | Th | RT | LT | Th | RT | W Side | E Side | N Side | S Side |
| 7:00-8:00 | 53 | 168 | 0 | 0 | 209 | 10 | 0 | 0 | 0 | 2 | 0 | 9 | 5 | 5 | 5 | 5 |
| 8:00-9:00 | 70 | 223 | 0 | 0 | 277 | 13 | 0 | 0 | 0 | 2 | 0 | 12 | 5 | 5 | 5 | 5 |
| 12:00-13:00 | 17 | 204 | 0 | 0 | 174 | 3 | 0 | 0 | 0 | 9 | 0 | 54 | 5 | 5 | 5 | 5 |
| 13:00-14:00 | 19 | 220 | 0 | 0 | 188 | 3 | 0 | 0 | 0 | 10 | 0 | 58 | 5 | 5 | 5 | 5 |
| 16:00-17:00 | 25 | 293 | 0 | 0 | 250 | 4 | 0 | 0 | 0 | 13 | 0 | 77 | 5 | 5 | 5 | 5 |
| 17:00-18:00 | 23 | 275 | 0 | 0 | 234 | 4 | 0 | 0 | 0 | 12 | 0 | 72 | 5 | 5 | 5 | 5 |
| Total (6-hour peak) | 207 | 1,383 | 0 | 0 | 1,332 | 37 | 0 | 0 | 0 | 48 | 0 | 282 | 30 | 30 | 30 | 30 |
| Average (6-hour peak) | 35 | 231 | 0 | 0 | 222 | 6 | 0 | 0 | 0 | 8 | 0 | 47 | 5 | 5 | 5 | 5 |



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NSDPW - Traffic Signal Warrant Analysis


| Road Authority: | NSDPW |
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| Count Date: | 2022 Nov 14, Mon |
| Date Entry Format: | (yyyy-mm-dd) |
|  |  |


| Lane Configuration |  | ち |  | $\begin{aligned} & \text { 硈 } \\ & \text { ob } \\ & \text { B } \end{aligned}$ |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\sim} \\ & \approx \\ & \underset{F}{F} \end{aligned}$ | $\begin{aligned} & \stackrel{\rightharpoonup}{\widetilde{v}} \\ & \stackrel{\rightharpoonup}{v} \\ & \hline \end{aligned}$ |  | E. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Trunk 2 | NB | 1 |  | 1 |  |  |  | 2,000 | 1 |
| Trunk 2 | SB |  |  |  |  | 1 |  | 2,000 | 1 |
| Parcel F Res Dwy | WB |  |  |  |  |  |  |  |  |
| Parcel F Res Dwy | EB |  |  |  | 1 |  |  |  |  |
| Are the Parcel F Res Dwy EB right turns significantly impeded by through movements? (y/n) |  |  |  |  |  |  | n |  |  |
|  |  |  |  |  |  |  | n |  |  |





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| ---: | :---: |
| City: | Mun. of East Hants |
| Analysis Date: | 2023 Apr 14, Fri |
| Count Date: | 2022 Nov 14, Mon |
| Date Entry Format: | (yyyy-mm-dd) |
|  |  |


| Lane Configuration |  | E c x | $\begin{aligned} & \leftrightarrows \\ & \stackrel{y}{*} \\ & \stackrel{I}{F} \end{aligned}$ |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{\sim} \\ & \text { * } \\ & \stackrel{\leftrightarrows}{2} \end{aligned}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| New Collector St | WB |  |  |  |  | 1 |  | 2,000 | 1 |
| New Collector St | EB | 1 |  | 1 |  |  |  | 2,000 | 1 |
| Parcel D Comm Dwy | NB |  |  |  |  |  |  |  |  |
| Parcel D Comm Dwy | SB |  |  |  | 1 |  |  |  |  |
| Are the Parcel D Comm Dwy SB right turns significantly impeded by through movements? (y/n) |  |  |  |  |  |  | n |  |  |
|  |  |  |  |  |  |  | n |  |  |


| Demographics |  |  |
| :--- | :---: | :---: |
| Elem. School/Mobility Challenged | $(\mathrm{y} / \mathrm{n})$ | n |
| Senior's Complex | $(\mathrm{y} / \mathrm{n})$ | n |
| Pathway to School | $(\mathrm{y} / \mathrm{n})$ | n |
| Metro Area Population | $(\#)$ | 20,000 |
| Central Business District | $(\mathrm{y} / \mathrm{n})$ | n |




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APPENDIX III Auxiliary Lane Warrant Results

## Left Turn Lane Warrant Analysis Background 2043 Traffic Volumes

 Trunk 2/WickWire South - Northbound Left TurnWeekday AM Peak Hour - MTO 2017 Design Supplement Exhibit 9A-8:


Advancing Traffic:
$V_{A}=213 \mathrm{vph}$
Warrant Not Met
$V_{\mathrm{L}}=57 \mathrm{vph}$
Left turns $=26.8 \%$

Weekday PM Peak Hour - MTO 2017 Design Supplement Exhibit 9A-9:


Advancing Traffic:
$\mathrm{V}_{\mathrm{A}}=503 \mathrm{vph}$
Warrant Met
$V_{L}=191 \mathrm{vph}$
Left turns = 38.0\%

## Left Turn Lane Warrant Analysis Background 2043 Traffic Volumes

 Trunk 2/WickWire North - Northbound Left TurnWeekday AM Peak Hour - MTO 2017 Design Supplement Exhibit 9A-7:


Advancing Traffic:
$\mathrm{V}_{\mathrm{A}}=139 \mathrm{vph}$
Warrant Not Met
$\mathrm{VL}=24 \mathrm{vph}$
Left turns = 17.3\%

Weekday PM Peak Hour - MTO 2017 Design Supplement Exhibit 9A-8:


Advancing Traffic:
$\mathrm{V}_{\mathrm{A}}=279 \mathrm{vph}$
Warrant Not Met
V L $=79 \mathrm{vph}$
Left turns = 28.3\%

# Left Turn Lane Warrant Analysis Total 2043 Traffic Volumes Trunk 2/WickWire North - Northbound Left Turn 

Weekday AM Peak Hour - MTO 2017 Design Supplement Exhibit 9A-7:


Advancing Traffic:
$\mathrm{V}_{\mathrm{A}}=382 \mathrm{vph}$
$\mathrm{V}_{\mathrm{L}}=79 \mathrm{vph}$
Warrant Met
Left turns $=20.7 \%$

Weekday PM Peak Hour - MTO 2017 Design Supplement Exhibit 9A-9:


Advancing Traffic:
$\mathrm{V}_{\mathrm{A}}=755 \mathrm{vph}$
Warrant Met
V = 264 vph
Left turns $=35.0 \%$

## Left Turn Lane Warrant Analysis Total 2043 Traffic Volumes Trunk 2/Road A - Northbound Left Turn

Weekday AM Peak Hour - MTO 2017 Design Supplement Exhibit 9A-9:


Advancing Traffic:
$\mathrm{V}_{\mathrm{A}}=306 \mathrm{vph}$
Warrant Met
$V_{L}=116 \mathrm{vph}$
Left turns $=37.9 \%$

Weekday PM Peak Hour - MTO 2017 Design Supplement Exhibit 9A-9:


Advancing Traffic:
$\mathrm{V}_{\mathrm{A}}=474 \mathrm{vph}$
Warrant Met
V L $=227 \mathrm{vph}$
Left turns = 47.9\%

## Left Turn Lane Warrant Analysis Total 2043 Traffic Volumes <br> Trunk 2/Parcel B Access - Northbound Left Turn

Weekday AM Peak Hour - MTO 2017 Design Supplement Exhibit 9A-8:


Advancing Traffic:
$\mathrm{V}_{\mathrm{A}}=293 \mathrm{vph}$
$\mathrm{V}_{\mathrm{L}}=70 \mathrm{vph}$
Warrant Not Met
Left turns $=23.9 \%$

Weekday PM Peak Hour - MTO 2017 Design Supplement Exhibit 9A-6:


Advancing Traffic:
$\mathrm{V}_{\mathrm{A}}=318 \mathrm{vph}$
Warrant Not Met
$\mathrm{V}_{\mathrm{L}}=25 \mathrm{vph}$
Left turns $=7.9 \%$

## Left Turn Lane Warrant Analysis Total 2043 Traffic Volumes <br> Trunk 2/Parcel F Access - Northbound Left Turn

Weekday AM Peak Hour - MTO 2017 Design Supplement Exhibit 9A-6:


Advancing Traffic:
$\mathrm{V}_{\mathrm{A}}=225 \mathrm{vph}$
$V_{\mathrm{L}}=21 \mathrm{vph}$
Warrant Not Met
Left turns $=9.3 \%$

Weekday PM Peak Hour - MTO 2017 Design Supplement Exhibit 9A-7:


Advancing Traffic:
$\mathrm{V}_{\mathrm{A}}=306 \mathrm{vph}$
Warrant Not Met
$\mathrm{V}_{\mathrm{L}}=53 \mathrm{vph}$
Left turns $=17.3 \%$

## Right Turn Lane Warrant Analysis Background 2043 Traffic Volumes Trunk 2/Wickwire South - Southbound Right Turn

Weekday AM Peak Hour - 70 km/h or less:


Advancing Traffic:
$\mathrm{V}_{\mathrm{A}}=297 \mathrm{vph}$

Weekday PM Peak Hour - 70 km/h or less:


## Right Turn Lane Warrant Analysis Background 2043 Traffic Volumes Trunk 2/Wickwire North - Southbound Right Turn

Weekday AM Peak Hour - 70 km/h or less:


Advancing Traffic: $\mathrm{V}_{\mathrm{A}}=162 \mathrm{vph}$

Weekday PM Peak Hour - 70 km/h or less:


Weekday AM Peak Hour - 70 km/h or less:


Advancing Traffic: $\mathrm{V}_{\mathrm{A}}=484 \mathrm{vph}$

Weekday PM Peak Hour - 70 km/h or less:


## Right Turn Lane Warrant Analysis <br> Total 2043 Traffic Volumes <br> Trunk 2/Wickwire North - Northbound Right Turn

Weekday AM Peak Hour - $70 \mathrm{~km} / \mathrm{h}$ or less:


Advancing Traffic: $\mathrm{V}_{\mathrm{A}}=382 \mathrm{vph}$

Weekday PM Peak Hour - $70 \mathrm{~km} / \mathrm{h}$ or less:


Advancing Traffic:
$\mathrm{V}_{\mathrm{A}}=755 \mathrm{vph}$

## Right Turn Lane Warrant Analysis <br> Total 2043 Traffic Volumes Trunk 2/Road A - Southbound Right Turn

Weekday AM Peak Hour - 70 km/h or less:


Advancing Traffic: $\mathrm{V}_{\mathrm{A}}=289 \mathrm{vph}$

Weekday PM Peak Hour - 70 km/h or less:


Advancing Traffic:
$\mathrm{V}_{\mathrm{A}}=327 \mathrm{vph}$

Weekday AM Peak Hour - 70 km/h or less:


Advancing Traffic: $\mathrm{V}_{\mathrm{A}}=290 \mathrm{vph}$

Weekday PM Peak Hour - 70 km/h or less:


Advancing Traffic:
$\mathrm{V}_{\mathrm{A}}=254 \mathrm{vph}$

Trunk 2/Parcel F Access - Southbound Right Turn

Weekday AM Peak Hour - 70 km/h or less:


Advancing Traffic:
$\mathrm{V}_{\mathrm{A}}=222 \mathrm{vph}$

Weekday PM Peak Hour - 70 km/h or less:


Advancing Traffic:
$\mathrm{V}_{\mathrm{A}}=234 \mathrm{vph}$

## APPENDIX IV Intersection operational analyses

## Lantz Connector Corridor Roundabout Results All Planning Horizons

## 1. Lantz Connector Road / Highway 102 Southbound Ramps



## Legs

Legs

| Leg | Name | Description | No yield line |
| :---: | :---: | :--- | :--- |
| WB | LantzWB |  |  |
| SB | OffRampSB |  |  |
| NB | OnRampNB |  |  |

Roundabout Geometry

| Leg | V-Approach road half-width <br> $(\mathbf{m})$ | E-Entry width <br> $(\mathbf{m})$ | $\mathbf{r}$ - Effective flare length <br> $(\mathbf{m})$ | R-Entry radius <br> $(\mathbf{m})$ | - Inscribed circle diameter <br> $(\mathbf{m})$ | PHI - Conflict (entry) angle <br> $($ deg $)$ | Entry <br> only | Exit <br> only |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WB | 3.50 | 4.00 | 30 | 30.0 | 450 |  |  |  |
| SB | 3.50 | 4.00 | 30.0 | 30.0 |  | 20 |  |  |
| NB |  |  |  |  |  | 20.0 |  |  |

Unsignalled Pedestrian Crossing Crossings

| Leg | Space between crossing and intersection <br> entry (Unsignalled Pedestrian Crossing) <br> (PEE) | Vehicles queueing on exit <br> (Unsignalled Pedestrian Crossing) <br> (PCE) | Central <br> Refuge | Crossing <br> data type | Crossing length <br> (entry side) (m) | Crossing time <br> (entry side) (s) | Crossing length <br> (exit side) (m) | Crossing time <br> (exit side) (s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WB | 1.00 | 1.00 | $\checkmark$ | Distance | 4.00 | 2.88 | 4.00 | 2.88 |
| SB | 1.00 | 1.00 | $\checkmark$ | Distance | 4.00 | 2.88 | 4.00 | 2.88 |
| NB |  | 1.00 | $\checkmark$ | Distance |  |  | 4.00 | 2.88 |

## 2. Lantz Connector Road / Highway 102 Northbound Ramps



|  | AM Vols |  |  |  |  |  |  |  |  | PM Vols |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Set <br> ID | Queue (Veh) |  | Delay (s) | V/C <br> Ratio | LOS | Intersection Delay (s) | Intersection LOS | Network Residual Capacity | Set <br> ID | Queue (Veh) |  | Delay (s) | V/C <br> Ratio | LOS | Intersection Delay (s) | $\begin{aligned} & \text { Intersection } \\ & \text { LOS } \end{aligned}$ | Network Residual Capacity |
|  | Existing Geometry - 2023 Baseline |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Leg WB | D1 | 0.2 | 0.5 | 3.61 | 0.17 | A | 3.43 | A | $\begin{gathered} 456 \% \\ {[\text { Leg WB] }} \end{gathered}$ | D2 | 0.1 | 0.5 | 3.36 | 0.11 | A | 3.19 | A | $\begin{gathered} 760 \% \\ {[\text { Leg WB] }} \end{gathered}$ |
| Leg EB |  | 0.1 | 0.5 | 3.14 | 0.05 | A |  |  |  |  | 0.1 | 0.5 | 3.19 | 0.06 | A |  |  |  |
| Leg NB |  | 0.0 | 0.5 | 3.08 | 0.00 | A |  |  |  |  | 0.0 | 0.5 | 3.11 | 0.00 | A |  |  |  |
|  | Existing Geometry - 2043 Bkgd |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Leg WB | D3 | 0.6 | 2.0 | 4.74 | 0.37 | A | 4.29 | A | $\begin{gathered} 158 \% \\ {[\text { Leg WB] }} \end{gathered}$ | D4 | 0.4 | 1.2 | 4.09 | 0.27 | A | 3.54 | A | $\begin{gathered} 256 \% \\ {[\text { Leg WB] }} \end{gathered}$ |
| Leg EB |  | 0.1 | 0.5 | 3.26 | 0.08 | A |  |  |  |  | 0.1 | 0.5 | 3.40 | 0.12 | A |  |  |  |
| Leg NB |  | 0.0 | 0.5 | 3.15 | 0.00 | A |  |  |  |  | 0.0 | 0.5 | 3.23 | 0.00 | A |  |  |  |
|  | Existing Geometry - 2043 Total |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Leg WB | D5 | 2.1 | 4.5 | 9.26 | 0.68 | A | 7.57 | A | $\begin{gathered} 40 \% \\ {[\text { Leg WB] }} \end{gathered}$ | D6 | 0.8 | 1.5 | 5.51 | 0.46 | A | 4.11 | A | $\begin{gathered} 108 \% \\ {\left[\begin{array}{l} \text { Leg } \end{array}\right.} \\ \text { WB] } \end{gathered}$ |
| Leg EB |  | 0.1 | 0.5 | 3.30 | 0.09 | A |  |  |  |  | 0.2 | 0.5 | 3.50 | 0.15 | A |  |  |  |
| Leg NB |  | 0.0 | 0.5 | 3.17 | 0.00 | A |  |  |  |  | 0.0 | 0.5 | 3.29 | 0.00 | A |  |  |  |

## Legs



| Leg | V - Approach road half-width (m) | $\begin{gathered} \text { E-Entry width } \\ (\mathrm{m}) \end{gathered}$ | $r$ - Effective flare length (m) | $\underset{(\mathrm{m})}{\mathrm{R}-\text { Entry radius }}$ | D - Inscribed circle diameter (m) | PHI - Conflict (entry) angle (deg) | $\begin{aligned} & \text { Entry } \\ & \text { only } \end{aligned}$ | $\begin{aligned} & \text { Exit } \\ & \text { only } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WB | 3.50 | 4.00 | 30.0 | 30.0 | 45.0 | 20.0 |  |  |
| SB |  |  |  |  |  |  |  | $\checkmark$ |
| EB | 3.50 | 4.00 | 30.0 | 30.0 | 45.0 | 20.0 |  |  |
| NB | 3.50 | 4.00 | 30.0 | 30.0 | 45.0 | 20.0 | $\checkmark$ |  |

Bypass

| Leg | Leg has bypass | Bypass utilisation (\%) |
| :---: | :---: | :---: |
| WB | $\checkmark$ | 100 |
| SB |  |  |
| EB |  |  |
| NB | $\checkmark$ | 100 |

Unsignalled Pedestrian Crossing Crossings

| Leg | Space between crossing and intersection entry (Unsignalled Pedestrian Crossing) (PCE) | Vehicles queueing on exit (Unsignalled Pedestrian Crossing) (PCE) | Central Refuge | Crossing data type | Crossing length (entry side) (m) | Crossing time (entry side) (s) | Crossing length (exit side) (m) | Crossing time (exit side) (s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| wB | 1.00 | 1.00 | $\checkmark$ | Distance | 4.00 | 2.86 | 4.00 | 2.86 |
| SB |  | 1.00 | $\checkmark$ | Distance |  |  | 4.00 | 2.86 |
| EB | 1.00 | 1.00 | $\checkmark$ | Distance | 4.00 | 2.88 | 4.00 | 2.86 |
| NB | 1.00 | 1.00 | $\checkmark$ | Distance | 4.00 | 2.86 | 4.00 | 2.86 |

## 3. Lantz Connector Road / Shaw Drive

†


|  | AM Vols |  |  |  |  |  |  |  |  | PM Vols |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { Set } \\ & \text { ID } \end{aligned}$ | Queue (Veh) | 95\% Queue (Veh) | Delay (5) | $\mathrm{V} / \mathrm{C}$ Ratio | LOS | Intersection Delay (s) | $\begin{aligned} & \text { Intersection } \\ & \text { LOS } \end{aligned}$ | Network Residual Capacity | $\begin{aligned} & \text { Set } \\ & \text { ID } \end{aligned}$ | Queue (Veh) | 95\% Queue (Veh) | Delay (5) | V/C Ratio | LOS | Intersection Delay (s) | $\begin{aligned} & \text { Intersection } \\ & \text { LOS } \end{aligned}$ | Network Residual Capacity |
|  | Existing Geometry - 2043 Bkgd |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Leg WB | D3 | 0.4 | 1.8 | 2.93 | 0.31 | A | 3.04 | A | $\begin{gathered} 126 \% \\ {[\text { Leg }} \\ \text { WB] } \end{gathered}$ | D4 | 0.2 | 0.5 | 2.31 | 0.17 | A | 3.48 | A | $69 \%$ <br> [Leg NB] |
| Leg EB |  | 0.1 | 0.5 | 2.01 | 0.12 | A |  |  |  |  | 0.6 | 2.0 | 2.81 | 0.37 | A |  |  |  |
| Leg NB |  | 0.3 | 1.3 | 4.35 | 0.22 | A |  |  |  |  | 0.5 | 1.9 | 6.80 | 0.33 | A |  |  |  |
|  | Existing Geometry - 2043 Total |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Leg WB | D5 | 1.5 | 2.1 | 5.72 | 0.60 | A | 4.74 | A | $\begin{gathered} 38 \% \\ {[\text { Leg WB] }} \end{gathered}$ | D6 | 0.5 | 1.9 | 3.01 | 0.32 | A | 4.86 | A | $\begin{gathered} 23 \% \\ {[\operatorname{Leg} N B]} \end{gathered}$ |
| Leg EB |  | 0.2 | 0.5 | 2.19 | 0.19 | A |  |  |  |  | 1.2 | 1.8 | 4.00 | 0.56 | A |  |  |  |
| Leg NB |  | 0.3 | 1.4 | 4.98 | 0.25 | A |  |  |  |  | 0.9 | 1.9 | 12.67 | 0.48 | B |  |  |  |

## Legs

Legs

| Leg | Name | Description | No yield line |
| :---: | :---: | :---: | :---: |
| WB | LantzWB |  |  |
| EB | LantzEB |  |  |
| NB | ShawNB |  |  |

Roundabout Geometry

| Leg | $\mathbf{V}$ - Approach road half-width <br> $(\mathbf{m})$ | $\mathbf{E}$ - Entry width <br> $(\mathbf{m})$ | $\mathbf{r}-$ Effective flare length <br> $(\mathbf{m})$ | $\mathbf{R}$ - Entry radius <br> $(\mathbf{m})$ | - Inscribed circle diameter <br> $(\mathbf{m})$ | PHI - Conflict (entry) angle <br> $($ deg $)$ | Entry <br> only |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WB | 7.00 | 7.00 | 0.0 | 30.0 | Exit <br> only |  |  |
| EB | 7.00 | 7.00 | 0.0 | 30.0 | 20.0 |  |  |
| NB | 3.50 | 4.00 | 30.0 | 30.0 | 50.0 |  |  |

Unsignalled Pedestrian Crossing Crossings

| Leg | Space between crossing and intersection entry (Unsignalled Pedestrian Crossing) (PCE) | Vehicles queueing on exit (Unsignalled Pedestrian Crossing) (PCE) | Central Refuge | Crossing data type | Crossing length (entry side) (m) | Crossing time (entry side) (s) | Crossing length (exit side) (m) | Crossing time (exit side) (s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WB | 1.00 | 1.00 | $\checkmark$ | Distance | 7.00 | 5.00 | 4.00 | 2.86 |
| EB | 1.00 | 1.00 | $\checkmark$ | Distance | 7.00 | 5.00 | 4.00 | 2.86 |
| NB | 1.00 | 1.00 | $\checkmark$ | Distance | 4.00 | 2.86 | 4.00 | 2.86 |

## 4. Lantz Connector Road / Trunk 2



|  | AM Vols |  |  |  |  |  |  |  |  | PM Vols |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { Set } \\ & \text { ID } \end{aligned}$ | Queue (Veh) | $\begin{aligned} & \text { 95\% } \\ & \text { Queue } \\ & \text { (Veh) } \end{aligned}$ | Delay (s) | $\mathrm{y} / \mathrm{C}$ Ratio | LOS | Intersection Delay (s) | Intersection LOS | Network Residual Capacity | $\begin{aligned} & \text { Set } \\ & \text { ID } \end{aligned}$ | Queue (Veh) | $95 \%$ Queue (Veh) | Delay (s) | v/C Ratio | LOS | Intersection Delay (s) | Intersection LOS | Network Residual Capacity |
|  | Existing Geometry - 2023 Baseline |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Leg WB | D1 | 0.0 | 0.5 | 3.41 | 0.01 | A | 2.39 | A | $\begin{gathered} 261 \% \\ \text { [Leg SB] } \end{gathered}$ | D2 | 0.0 | 0.5 | 4.25 | 0.03 | A | 2.37 | A | $\begin{gathered} 211 \% \\ {[\text { Leg WE] }} \end{gathered}$ |
| Leg SB |  | 0.3 | 1.4 | 2.70 | 0.26 | A |  |  |  |  | 0.2 | 0.5 | 2.41 | 0.17 | A |  |  |  |
| Leg EB |  | 0.1 | 0.5 | 1.99 | 0.08 | A |  |  |  |  | 0.3 | 0.8 | 2.29 | 0.21 | A |  |  |  |
| Leg NB |  | 0.1 | 0.5 | 1.93 | 0.10 | A |  |  |  |  | 0.2 | 0.5 | 2.27 | 0.16 | A |  |  |  |
|  | Existing Geometry - 2043 Bkgd |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Leg WB | D3 | 0.0 | 0.5 | 3.66 | 0.02 | A | 3.12 | A | $\begin{gathered} 109 \% \\ {[\text { Leg SE] }} \end{gathered}$ | D4 | 0.0 | 0.5 | 5.77 | 0.04 | A | 2.94 | A | $90 \%$[Leg WB] |
| Leg SB |  | 0.8 | 1.5 | 3.71 | 0.45 | A |  |  |  |  | 0.4 | 1.6 | 2.89 | 0.30 | A |  |  |  |
| Leg EB |  | 0.2 | 0.5 | 2.22 | 0.13 | A |  |  |  |  | 0.5 | 2.1 | 2.90 | 0.35 | A |  |  |  |
| Leg NB |  | 0.1 | 0.5 | 2.05 | 0.13 | A |  |  |  |  | 0.4 | 1.4 | 2.90 | 0.29 | A |  |  |  |
|  | Existing Geometry - 2043 Total |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Leg WB | D5 | 0.0 | 0.5 | 4.14 | 0.02 | A | 6.01 | A | $\begin{gathered} 30 \% \\ {[\operatorname{Leg} \text { SE] }} \end{gathered}$ | D6 | 0.1 | 0.5 | 10.15 | 0.07 | B | 4.34 | A | $\begin{gathered} 30 \% \\ {[\text { Leg WB] }} \end{gathered}$ |
| Leg SB |  | 2.9 | 7.4 | 7.94 | 0.75 | A |  |  |  |  | 1.0 | 1.5 | 4.00 | 0.49 | A |  |  |  |
| Leg EB |  | 0.3 | 1.2 | 2.58 | 0.22 | A |  |  |  |  | 1.3 | 1.9 | 4.54 | 0.57 | A |  |  |  |
| Leg NB |  | 0.2 | 0.5 | 2.27 | 0.17 | A |  |  |  |  | 0.7 | 1.5 | 4.24 | 0.42 | A |  |  |  |

## Legs

Legs

| Leg | Name | Description | No yield line |
| :---: | :---: | :--- | :--- |
| WB | ClayWB |  |  |
| SB | TK2SB |  |  |
| EB | LantzEB |  |  |
| NB | TK2NB |  |  |

Roundabout Geometry

| Leg | V-Approach road half-width <br> $(\mathbf{m})$ | E-Entry width <br> $(\mathbf{m})$ | $\mathbf{r}$ - Effective flare length <br> $(\mathbf{m})$ | R - Entry radius <br> $(\mathbf{m})$ | D - Inscribed circle diameter <br> $(\mathbf{m})$ | PHI - Conflict (entry) angle <br> $(\mathbf{d e g})$ | Entry <br> only |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WB | 3.50 | 4.00 | 30.0 | 30.0 | 50.0 |  |  |
| SB | 3.50 | 7.00 | 30.0 | 30.0 | 50.0 |  |  |
| EB | 7.00 | 7.00 | 0.0 | 30.0 |  |  |  |
| NB | 7.00 | 7.00 | 0.0 | 30.0 |  |  |  |

## Unsignalled Pedestrian Crossing Crossings

| Leg | Space between crossing and intersection entry (Unsignalled Pedestrian Crossing) (PCE) | Vehicles queueing on exit (Unsignalled Pedestrian Crossing) (PCE) | Central Refuge | Crossing data type | Crossing length (entry side) (m) | Crossing time (entry side) (s) | Crossing length (exit side) (m) | Crossing time (exit side) (s) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WB | 1.00 | 1.00 | $\checkmark$ | Distance | 4.00 | 2.86 | 4.00 | 2.86 |
| SB | 1.00 | 1.00 | $\checkmark$ | Distance | 7.00 | 5.00 | 7.00 | 5.00 |
| EB | 1.00 | 1.00 | $\checkmark$ | Distance | 7.00 | 5.00 | 4.00 | 2.88 |
| NB | 1.00 | 1.00 | $\checkmark$ | Distance | 7.00 | 5.00 | 4.00 | 2.86 |

## Trunk 2 Corridor Existing 2023 Results

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 25 | 4 | 90 | 11 | 2 | 140 |
| Future Vol, veh/h | 25 | 4 | 90 | 11 | 2 | 140 |
| Conflicting Peds, \#/hr | 1 | 1 | 0 | 1 | 1 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 27 | 4 | 98 | 12 | 2 | 152 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.5 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 11 | 4 | 154 | 25 | 2 | 102 |
| Future Vol, veh/h | 11 | 4 | 154 | 25 | 2 | 102 |
| Conflicting Peds, \#/hr | 1 | 1 | 0 | 1 | 1 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 12 | 4 | 167 | 27 | 2 | 111 |



## Trunk 2 Corridor

## 2043 Future Background Scenario Results




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 4 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | i | $\mathbf{7}$ |  | 4 | $\mathbf{b}$ |  |
| Traffic Vol, veh/h | 12 | 111 | 191 | 213 | 198 | 12 |
| Future Vol, veh/h | 12 | 111 | 191 | 213 | 198 | 12 |
| Conflicting Peds, \#/hr | 5 | 5 | 5 | 0 | 0 | 5 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 20 | 40 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 5 | 5 | 5 | 5 | 5 | 5 |
| Mvmt Flow | 13 | 121 | 208 | 232 | 215 | 13 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 3.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  | \$ |  |  | ¢ |  | ${ }^{7}$ | F |  | \% | $\hat{\dagger}$ |  |  |
| Traffic Vol, veh/h | 10 | 1 | 75 | 28 | 1 | 5 | 24 | 103 | 12 | 2 | 156 | 4 |  |
| Future Vol, veh/h | 10 | 1 | 75 | 28 | 1 | 5 | 24 | 103 | 12 | 2 | 156 | 4 |  |
| Conflicting Peds, \#/hr | 5 | 0 | 5 | 5 | 0 | 5 | 5 | 0 | 5 | 5 | 0 | 5 |  |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |  |
| Storage Length | - | - | - | - | - | - | 15 | - | - | 15 | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - |  | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |  |
| Mvmt Flow | 11 | 1 | 82 | 30 | 1 | 5 | 26 | 112 | 13 | 2 | 170 | 4 |  |



HCM 6th TWSC
6: Tk 2 \& Wickwire North/Robert Scott

|  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\frac{\text { Intersection }}{\text { Int Delay s/veh } 29}$ |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | \& |  | ${ }^{*}$ | 个 |  | ${ }^{7}$ | 个 |  |
| Traffic Vol, veh/h | 6 | 1 | 46 | 12 | 1 | 5 | 79 | 172 | 28 | 2 | 117 | 12 |
| Future Vol, veh/h | 6 | 1 | 46 | 12 | 1 | 5 | 79 | 172 | 28 | 2 | 117 | 12 |
| Conflicting Peds, \#/hr | 5 | 0 | 5 | 5 | 0 | 5 | 5 | 0 | 5 | 5 | 0 | 5 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | 15 | - | - | 15 | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| Mvmt Flow | 7 | 1 | 50 | 13 | 1 | 5 | 86 | 187 | 30 | 2 | 127 | 13 |



## Trunk 2 Corridor 2043 Future Total Scenario Results



|  |  |  |  |  | a |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
|  |  |  |  |  |  |  |

Splits and Phases: 5: Tk 2 \& Wickwire South


|  | 4 | $\cdots$ | 4 |  |  | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | F' | ${ }^{1}$ | 4 | 4 | 「' |
| Traffic Volume (vph) | 51 | 131 | 225 | 749 | 508 | 65 |
| Future Volume (vph) | 51 | 131 | 225 | 749 | 508 | 65 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | 15.0 | 30.0 |  |  | 30.0 |
| Storage Lanes | 1 | 1 | 1 |  |  | 1 |
| Taper Length (m) | 20.0 |  | 20.0 |  |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | 0.99 | 0.96 |  |  |  | 0.97 |
| Frt |  | 0.850 |  |  |  | 0.850 |
| Flt Protected | 0.950 |  | 0.950 |  |  |  |
| Satd. Flow (prot) | 1700 | 1521 | 1700 | 1789 | 1789 | 1521 |
| Flt Permitted | 0.950 |  | 0.227 |  |  |  |
| Satd. Flow (perm) | 1681 | 1461 | 406 | 1789 | 1789 | 1468 |
| Right Turn on Red |  | Yes |  |  |  | Yes |
| Satd. Flow (RTOR) |  | 142 |  |  |  | 51 |
| Link Speed (k/h) | 50 |  |  | 60 | 60 |  |
| Link Distance (m) | 234.3 |  |  | 363.0 | 194.0 |  |
| Travel Time (s) | 16.9 |  |  | 21.8 | 11.6 |  |
| Confl. Peds. (\#/hr) | 5 | 5 | 5 |  |  | 5 |
| Confl. Bikes (\#/hr) |  | 5 |  |  |  | 5 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 55 | 142 | 245 | 814 | 552 | 71 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |
| Lane Group Flow (vph) | 55 | 142 | 245 | 814 | 552 | 71 |
| Turn Type | Prot | Perm | pm+pt | NA | NA | Perm |
| Protected Phases | 4 |  | 5 | 2 | 6 |  |
| Permitted Phases |  | 4 | 2 |  |  | 6 |
| Detector Phase | 4 | 4 | 5 | 2 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 | 6.0 | 10.0 | 10.0 | 10.0 |
| Minimum Split (s) | 26.0 | 26.0 | 12.0 | 26.0 | 26.0 | 26.0 |
| Total Split (s) | 26.0 | 26.0 | 16.0 | 64.0 | 48.0 | 48.0 |
| Total Split (\%) | 28.9\% | 28.9\% | 17.8\% | 71.1\% | 53.3\% | 53.3\% |
| Maximum Green (s) | 20.0 | 20.0 | 10.0 | 58.0 | 42.0 | 42.0 |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Lead/Lag |  |  | Lead |  | Lag | Lag |
| Lead-Lag Optimize? |  |  | Yes |  | Yes | Yes |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None | Min | Min | Min | Min |
| Walk Time (s) | 8.0 | 8.0 |  | 8.0 | 8.0 | 8.0 |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 12.0 | 12.0 | 12.0 |
| Pedestrian Calls (\#/hr) | 5 | 5 |  | 5 | 5 | 5 |
| Act Effct Green (s) | 12.3 | 12.3 | 42.8 | 44.9 | 25.9 | 25.9 |
| Actuated g/C Ratio | 0.20 | 0.20 | 0.68 | 0.72 | 0.41 | 0.41 |
| v/c Ratio | 0.16 | 0.35 | 0.50 | 0.63 | 0.75 | 0.11 |


|  | 4 |  | 4 | $\dagger$ | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Control Delay | 27.1 | 8.5 | 8.8 | 10.4 | 23.9 | 6.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 27.1 | 8.5 | 8.8 | 10.4 | 23.9 | 6.1 |
| LOS | C | A | A | B | C | A |
| Approach Delay | 13.7 |  |  | 10.1 | 21.9 |  |
| Approach LOS | B |  |  | B | C |  |
| Queue Length 50th (m) | 5.2 | 0.0 | 8.9 | 46.6 | 49.8 | 1.3 |
| Queue Length 95th (m) | 15.9 | 12.9 | 23.7 | 114.8 | 97.5 | 8.0 |
| Internal Link Dist (m) | 210.3 |  |  | 339.0 | 170.0 |  |
| Turn Bay Length (m) |  | 15.0 | 30.0 |  |  | 30.0 |
| Base Capacity (vph) | 595 | 603 | 504 | 1585 | 1247 | 1039 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.09 | 0.24 | 0.49 | 0.51 | 0.44 | 0.07 |
| Intersection Summary |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |
| Cycle Length: 90 |  |  |  |  |  |  |
| Actuated Cycle Length: 62.6 |  |  |  |  |  |  |
| Natural Cycle: 65 |  |  |  |  |  |  |
| Control Type: Actuated-Uncoordinated |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.75 |  |  |  |  |  |  |
| Intersection Signal Delay: 14.3 |  |  |  |  | sectio | OS: B |
| Intersection Capacity Utilization 63.8\% |  |  |  | ICU Level of Service B |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |

Splits and Phases: 5: Tk 2 \& Wickwire South


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 7.2 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |  |
| Lane Configurations |  | ¢ |  |  | $\uparrow$ |  | \% | $\hat{\beta}$ |  | \% | $\hat{\square}$ |  |  |
| Traffic Vol, veh/h | 10 | 1 | 243 | 28 | 1 | 5 | 79 | 291 | 12 | 2 | 478 | 4 |  |
| Future Vol, veh/h | 10 | 1 | 243 | 28 | 1 | 5 | 79 | 291 | 12 | 2 | 478 | 4 |  |
| Conflicting Peds, \#/hr | 5 | 0 | 5 | 5 | 0 | 5 | 5 | 0 | 5 | 5 | 0 | 5 |  |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |  |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |  |
| Storage Length | - | - | - | - | - | - | 15 | - | - | 15 | - | - |  |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |  |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |  |
| Heavy Vehicles, \% | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |  |
| Mvmt Flow | 11 | 1 | 264 | 30 | 1 | 5 | 86 | 316 | 13 | 2 | 520 | 4 |  |



HCM 6th TWSC
6: Tk 2 \& Wickwire North/Robert Scott

| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 5.1 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * |  |  | \& |  | ${ }^{7}$ | $\uparrow$ |  | ${ }^{1 /}$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 6 | 1 | 157 | 12 | 1 | 5 | 264 | 463 | 28 | 2 | 369 | 12 |
| Future Vol, veh/h | 6 | 1 | 157 | 12 | 1 | 5 | 264 | 463 | 28 | 2 | 369 | 12 |
| Conflicting Peds, \#/hr | 5 | 0 | 5 | 5 | 0 | 5 | 5 | 0 | 5 | 5 | 0 | 5 |
| Sign Control | Stop | Stop | Stop | Stop | Stop | Stop | Free | Free | Free | Free | Free | Free |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | - | - | - | - | - | - | 15 | - | - | 15 | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| Mvmt Flow | 7 | 1 | 171 | 13 | 1 | 5 | 287 | 503 | 30 | 2 | 401 | 13 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 6.8 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | T | $\mathbf{7}$ |  | 4 | $\mathbf{b}$ |  |
| Traffic Vol, veh/h | 103 | 266 | 116 | 190 | 218 | 71 |
| Future Vol, veh/h | 103 | 266 | 116 | 190 | 218 | 71 |
| Conflicting Peds, \#/hr | 5 | 5 | 5 | 0 | 0 | 5 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 15 | 15 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 5 | 5 | 5 | 5 | 5 | 5 |
| Mvmt Flow | 112 | 289 | 126 | 207 | 237 | 77 |







| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |





|  | EB | NB | SB |
| :--- | :---: | :---: | :---: |
| Approach | 0.7 | 0 |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1296 | -696 | - | - |  |
| HCM Lane V/C Ratio | 0.018 | -0.145 | - | - |  |
| HCM Control Delay (s) | 7.8 | 0 | 11 | - | - |
| HCM Lane LOS | A | A | B | - | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | 0.5 | - | - |


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.5 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | * |  |  | $\uparrow$ | F |  |
| Traffic Vol, veh/h | 9 | 34 | 53 | 253 | 220 | 14 |
| Future Vol, veh/h | 9 | 34 | 53 | 253 | 220 | 14 |
| Conflicting Peds, \#/hr | 5 | 5 | 5 | 0 | 0 | 5 |
| Sign Control Stor | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | \# 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 5 | 5 | 5 | 5 | 5 | 5 |
| Mvmt Flow | 10 | 37 | 58 | 275 | 239 | 15 |



|  | EB | NB | SB |
| :--- | :---: | :---: | :---: |
| Approach | 11 | 0 |  |
| HCM Control Delay, s | 11 | 1.4 |  |


| Minor Lane/Major Mvmt | NBL | NBT EBLn1 | SBT | SBR |  |
| :--- | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 1282 | -645 | - | - |  |
| HCM Lane V/C Ratio | 0.045 | -0.072 | - | - |  |
| HCM Control Delay (s) | 7.9 | 0 | 11 | - | - |
| HCM Lane LOS | A | A | B | - | - |
| HCM 95th \%tile Q(veh) | 0.1 | - | 0.2 | - | - |



| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | ---: | :--- | :--- | :--- | :--- | ---: |
| Conflicting Flow All | 208 | 0 | - | 0 | 622 | 146 |
| $\quad$ Stage 1 | - | - | - | - | 141 | - |
| Stage 2 | - | - | - | - | 481 | - |
| Critical Hdwy | 4.15 | - | - | -6.45 | 6.25 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.45 | - |
| Critical Hdwy Stg 2 | - | - | - | -5.45 | - |  |
| Follow-up Hdwy | 2.245 | - | - | -3.545 | 3.345 |  |
| Pot Cap-1 Maneuver | 1345 | - | - | - | 446 | 893 |
| $\quad$ Stage 1 | - | - | - | - | 879 | - |
| $\quad$ Stage 2 | - | - | - | - | 616 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1339 | - | - | - | 401 | 885 |
| Mov Cap-2 Maneuver | - | - | - | - | 401 | - |
| Stage 1 | - | - | - | - | 794 | - |
| Stage 2 | - | - | - | - | 613 | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 2.8 | 0 | 20 |
| HCM LOS |  |  | C |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1339 | - | - | -467 |
| HCM Lane V/C Ratio | 0.092 | - | - | -0.493 |
| HCM Control Delay (s) | 8 | - | - | - |
| HCM Lane LOS | A | - | - | - |
| HCM 95th \%tile Q(veh) | 0.3 | - | - | - |
| C | 2.7 |  |  |  |



| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | ---: | :--- | ---: | :--- | ---: | ---: |
| Conflicting Flow All | 354 | 0 | - | 0 | 580 | 297 |
| $\quad$ Stage 1 | - | - | - | - | 292 | - |
| Stage 2 | - | - | - | - | 288 | - |
| Critical Hdwy | 4.15 | - | - | - | 6.45 | 6.25 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.45 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.45 | - |
| Follow-up Hdwy | 2.245 | - | - | -3.545 | 3.345 |  |
| Pot Cap-1 Maneuver | 1188 | - | - | - | 472 | 735 |
| $\quad$ Stage 1 | - | - | - | - | 751 | - |
| $\quad$ Stage 2 | - | - | - | - | 754 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1182 | - | - | - | 438 | 728 |
| Mov Cap-2 Maneuver | - | - | - | - | 438 | - |
| Stage 1 | - | - | - | -700 | - |  |
| Stage 2 | - | - | - | - | 750 | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 2.9 | 0 | 15.5 |
| HCM LOS |  |  | C |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1182 | - | - | -533 |
| HCM Lane V/C Ratio | 0.063 | - | - | -0.359 |
| HCM Control Delay (s) | 8.2 | - | - | -15.5 |
| HCM Lane LOS | A | - | - | - |
| HCM 95th \%tile Q(veh) | 0.2 | - | - | - |
| H | 1.6 |  |  |  |

Trunk 2 Corridor Sensitivity Analysis Long-Term Full Build-Out Scenario Results

|  | 4 |  | 4 |  |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | T | ${ }^{1}$ | 4 | 中 ${ }^{\text {a }}$ |  |
| Traffic Volume (vph) | 86 | 605 | 208 | 406 | 926 | 38 |
| Future Volume (vph) | 86 | 605 | 208 | 406 | 926 | 38 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | 15.0 | 0.0 |  |  | 30.0 |
| Storage Lanes | 1 | 1 | 1 |  |  | 0 |
| Taper Length (m) | 20.0 |  | 20.0 |  |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor | 0.99 | 0.98 |  |  | 1.00 |  |
| Frt |  | 0.850 |  |  | 0.994 |  |
| Flt Protected | 0.950 |  | 0.950 |  |  |  |
| Satd. Flow (prot) | 1700 | 1521 | 1700 | 1789 | 3375 | 0 |
| Flt Permitted | 0.950 |  | 0.114 |  |  |  |
| Satd. Flow (perm) | 1681 | 1488 | 204 | 1789 | 3375 | 0 |
| Right Turn on Red |  | Yes |  |  |  | Yes |
| Satd. Flow (RTOR) |  | 285 |  |  | 5 |  |
| Link Speed (k/h) | 50 |  |  | 60 | 60 |  |
| Link Distance (m) | 234.3 |  |  | 363.0 | 194.0 |  |
| Travel Time (s) | 16.9 |  |  | 21.8 | 11.6 |  |
| Confl. Peds. (\#/hr) | 5 | 5 | 5 |  |  | 5 |
| Confl. Bikes (\#/hr) |  | 5 |  |  |  | 5 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 93 | 658 | 226 | 441 | 1007 | 41 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |
| Lane Group Flow (vph) | 93 | 658 | 226 | 441 | 1048 | 0 |
| Turn Type | Prot | Perm | pm+pt | NA | NA |  |
| Protected Phases | 4 |  | 5 | 2 | 6 |  |
| Permitted Phases |  | 4 | 2 |  |  |  |
| Detector Phase | 4 | 4 | 5 | 2 | 6 |  |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 | 6.0 | 10.0 | 10.0 |  |
| Minimum Split (s) | 26.0 | 26.0 | 12.0 | 26.0 | 26.0 |  |
| Total Split (s) | 38.0 | 38.0 | 16.0 | 52.0 | 36.0 |  |
| Total Split (\%) | 42.2\% | 42.2\% | 17.8\% | 57.8\% | 40.0\% |  |
| Maximum Green (s) | 32.0 | 32.0 | 10.0 | 46.0 | 30.0 |  |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  |
| Lead/Lag |  |  | Lead |  | Lag |  |
| Lead-Lag Optimize? |  |  | Yes |  | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None | Min | Min | Min |  |
| Walk Time (s) | 8.0 | 8.0 |  | 8.0 | 8.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 5 | 5 |  | 5 | 5 |  |
| Act Effct Green (s) | 29.3 | 29.3 | 45.2 | 45.2 | 29.1 |  |
| Actuated g/C Ratio | 0.34 | 0.34 | 0.52 | 0.52 | 0.34 |  |
| v/c Ratio | 0.16 | 0.95 | 0.81 | 0.47 | 0.92 |  |



Splits and Phases: 5: Tk 2 \& Wickwire South


|  | 4 | $\geqslant$ | 4 |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | F | ${ }^{4}$ | 4 | 中 ${ }^{\text {a }}$ |  |
| Traffic Volume (vph) | 81 | 393 | 662 | 915 | 611 | 92 |
| Future Volume (vph) | 81 | 393 | 662 | 915 | 611 | 92 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (m) | 0.0 | 15.0 | 0.0 |  |  | 30.0 |
| Storage Lanes | 1 | 1 | 1 |  |  | 0 |
| Taper Length (m) | 20.0 |  | 20.0 |  |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor | 0.99 | 0.98 |  |  | 0.99 |  |
| Frt |  | 0.850 |  |  | 0.980 |  |
| Flt Protected | 0.950 |  | 0.950 |  |  |  |
| Satd. Flow (prot) | 1700 | 1521 | 1700 | 1789 | 3315 | 0 |
| Flt Permitted | 0.950 |  | 0.154 |  |  |  |
| Satd. Flow (perm) | 1681 | 1485 | 276 | 1789 | 3315 | 0 |
| Right Turn on Red |  | Yes |  |  |  | Yes |
| Satd. Flow (RTOR) |  | 427 |  |  | 17 |  |
| Link Speed (k/h) | 50 |  |  | 60 | 60 |  |
| Link Distance ( m ) | 234.3 |  |  | 363.0 | 194.0 |  |
| Travel Time (s) | 16.9 |  |  | 21.8 | 11.6 |  |
| Confl. Peds. (\#/hr) | 5 | 5 | 5 |  |  | 5 |
| Confl. Bikes (\#/hr) |  | 5 |  |  |  | 5 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 88 | 427 | 720 | 995 | 664 | 100 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |
| Lane Group Flow (vph) | 88 | 427 | 720 | 995 | 764 | 0 |
| Turn Type | Prot | Perm | pm+pt | NA | NA |  |
| Protected Phases | 4 |  | 5 | 2 | 6 |  |
| Permitted Phases |  | 4 | 2 |  |  |  |
| Detector Phase | 4 | 4 | 5 | 2 | 6 |  |
| Switch Phase |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 | 6.0 | 10.0 | 10.0 |  |
| Minimum Split (s) | 26.0 | 26.0 | 12.0 | 26.0 | 26.0 |  |
| Total Split (s) | 26.0 | 26.0 | 38.0 | 64.0 | 26.0 |  |
| Total Split (\%) | 28.9\% | 28.9\% | 42.2\% | 71.1\% | 28.9\% |  |
| Maximum Green (s) | 20.0 | 20.0 | 32.0 | 58.0 | 20.0 |  |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time (s) | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  |
| Lead/Lag |  |  | Lead |  | Lag |  |
| Lead-Lag Optimize? |  |  | Yes |  | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Recall Mode | None | None | Min | Min | Min |  |
| Walk Time (s) | 8.0 | 8.0 |  | 8.0 | 8.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 |  | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 5 | 5 |  | 5 | 5 |  |
| Act Effct Green (s) | 12.0 | 12.0 | 58.1 | 58.1 | 20.0 |  |
| Actuated g/C Ratio | 0.15 | 0.15 | 0.71 | 0.71 | 0.24 |  |
| v/c Ratio | 0.35 | 0.73 | 0.96 | 0.79 | 0.93 |  |



Splits and Phases: 5: Tk 2 \& Wickwire South


|  | 4 |  | 7 | 4 |  |  | 4 | $\dagger$ | \% | $V$ |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 |  | $\ddagger$ |  | ${ }^{7}$ | 个 |  | ${ }^{1}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 34 | 1 | 413 | 28 | 1 | 5 | 138 | 315 | 12 | 2 | 485 | 13 |
| Future Volume (vph) | 34 | 1 | 413 | 28 | 1 | 5 | 138 | 315 | 12 | 2 | 485 | 13 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Storage Length (m) | 0.0 |  | 15.0 | 0.0 |  | 0.0 | 30.0 |  | 0.0 | 15.0 |  | 0.0 |
| Storage Lanes | 0 |  | 1 | 0 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 2.5 |  |  | 2.5 |  |  | 20.0 |  |  | 20.0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 | 0.96 |  | 0.99 |  |  | 1.00 |  | 0.99 | 1.00 |  |
| Frt |  |  | 0.850 |  | 0.981 |  |  | 0.995 |  |  | 0.996 |  |
| Flt Protected |  | 0.954 |  |  | 0.960 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1707 | 1521 | 0 | 1676 | 0 | 1700 | 1778 | 0 | 1700 | 1781 | 0 |
| Flt Permitted |  | 0.715 |  |  | 0.756 |  | 0.292 |  |  | 0.549 |  |  |
| Satd. Flow (perm) | 0 | 1266 | 1463 | 0 | 1308 | 0 | 523 | 1778 | 0 | 976 | 1781 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 390 |  | 5 |  |  | 4 |  |  | 2 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 154.6 |  |  | 127.5 |  |  | 136.8 |  |  | 419.6 |  |
| Travel Time (s) |  | 11.1 |  |  | 9.2 |  |  | 8.2 |  |  | 25.2 |  |
| Confl. Peds. (\#/hr) | 5 |  | 5 | 5 |  | 5 | 5 |  | 5 | 5 |  | 5 |
| Confl. Bikes (\#/hr) |  |  | 5 |  |  | 5 |  |  | 5 |  |  | 5 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 5\% | 5\% | 5\% | 5\% | 5\% | 5\% | 5\% | 5\% | 5\% | 5\% | 5\% | 5\% |
| Adj. Flow (vph) | 37 | 1 | 449 | 30 | 1 | 5 | 150 | 342 | 13 | 2 | 527 | 14 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 38 | 449 | 0 | 36 | 0 | 150 | 355 | 0 | 2 | 541 | 0 |
| Turn Type | Perm | NA | Perm | Perm | NA |  | pm+pt | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 | 4 | 8 | 8 |  | 5 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |  | 6.0 | 10.0 |  | 10.0 | 10.0 |  |
| Minimum Split (s) | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 |  | 12.0 | 26.0 |  | 26.0 | 26.0 |  |
| Total Split (s) | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 |  | 16.0 | 60.0 |  | 44.0 | 44.0 |  |
| Total Split (\%) | 33.3\% | 33.3\% | 33.3\% | 33.3\% | 33.3\% |  | 17.8\% | 66.7\% |  | 48.9\% | 48.9\% |  |
| Maximum Green (s) | 24.0 | 24.0 | 24.0 | 24.0 | 24.0 |  | 10.0 | 54.0 |  | 38.0 | 38.0 |  |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) |  | 0.0 | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 6.0 | 6.0 |  | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lead |  |  | Lag | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes |  |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None | None | None | None |  | None | Max |  | Max | Max |  |
| Walk Time (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |  |  | 8.0 |  | 8.0 | 8.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 |  |  | 12.0 |  | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 5 | 5 | 5 | 5 | 5 |  |  | 5 |  | 5 | 5 |  |
| Act Effct Green (s) |  | 13.7 | 13.7 |  | 13.7 |  | 54.2 | 54.2 |  | 40.3 | 40.3 |  |


| 4 | $\rightarrow$ |  | 7 |  |  | , | $\dagger$ | $p$ |  | $\dagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Actuated g/C Ratio | 0.17 | 0.17 |  | 0.17 |  | 0.68 | 0.68 |  | 0.50 | 0.50 |  |
| v/c Ratio | 0.18 | 0.78 |  | 0.16 |  | 0.32 | 0.29 |  | 0.00 | 0.60 |  |
| Control Delay | 29.2 | 16.0 |  | 25.8 |  | 7.4 | 6.8 |  | 13.5 | 19.3 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 29.2 | 16.0 |  | 25.8 |  | 7.4 | 6.8 |  | 13.5 | 19.3 |  |
| LOS | C | B |  | C |  | A | A |  | B | B |  |
| Approach Delay | 17.0 |  |  | 25.8 |  |  | 6.9 |  |  | 19.3 |  |
| Approach LOS | B |  |  | C |  |  | A |  |  | B |  |
| Queue Length 50th (m) | 4.6 | 7.2 |  | 3.7 |  | 5.2 | 14.0 |  | 0.1 | 45.2 |  |
| Queue Length 95th (m) | 11.6 | 34.4 |  | 10.4 |  | 17.0 | 39.8 |  | 1.4 | 104.1 |  |
| Internal Link Dist (m) | 130.6 |  |  | 103.5 |  |  | 112.8 |  |  | 395.6 |  |
| Turn Bay Length (m) |  | 15.0 |  |  |  | 30.0 |  |  | 15.0 |  |  |
| Base Capacity (vph) | 381 | 713 |  | 397 |  | 502 | 1206 |  | 491 | 898 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.10 | 0.63 |  | 0.09 |  | 0.30 | 0.29 |  | 0.00 | 0.60 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 90 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 80 |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 65 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.78 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 14.8 Intersection LOS: B |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 77.0\% ICU Level of Service D |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 6: Tk 2 \& Wickwire North/Robert Scott


|  | 4 | $\rightarrow$ | 7 | 7 |  |  |  | 4 | 7 |  |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | 「 |  | \$ |  | ${ }^{1}$ | F |  | ${ }^{*}$ | $\uparrow$ |  |
| Traffic Volume (vph) | 21 | 1 | 265 | 12 | 1 | 5 | 445 | 478 | 28 | 2 | 391 | 39 |
| Future Volume (vph) | 21 | 1 | 265 | 12 | 1 | 5 | 445 | 478 | 28 | 2 | 391 | 39 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Storage Length (m) | 0.0 |  | 15.0 | 0.0 |  | 0.0 | 90.0 |  | 0.0 | 15.0 |  | 0.0 |
| Storage Lanes | 0 |  | 1 | 0 |  | 0 | 1 |  | 0 | 1 |  | 0 |
| Taper Length (m) | 2.5 |  |  | 2.5 |  |  | 20.0 |  |  | 20.0 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor |  | 0.99 | 0.96 |  | 0.98 |  | 1.00 | 1.00 |  | 0.99 | 1.00 |  |
| Frt |  |  | 0.850 |  | 0.964 |  |  | 0.992 |  |  | 0.987 |  |
| Flt Protected |  | 0.954 |  |  | 0.967 |  | 0.950 |  |  | 0.950 |  |  |
| Satd. Flow (prot) | 0 | 1707 | 1521 | 0 | 1651 | 0 | 1700 | 1772 | 0 | 1700 | 1761 | 0 |
| Flt Permitted |  | 0.737 |  |  | 0.816 |  | 0.352 |  |  | 0.458 |  |  |
| Satd. Flow (perm) | 0 | 1305 | 1461 | 0 | 1383 | 0 | 628 | 1772 | 0 | 815 | 1761 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 288 |  | 5 |  |  | 6 |  |  | 7 |  |
| Link Speed (k/h) |  | 50 |  |  | 50 |  |  | 60 |  |  | 60 |  |
| Link Distance (m) |  | 154.6 |  |  | 127.5 |  |  | 136.8 |  |  | 419.6 |  |
| Travel Time (s) |  | 11.1 |  |  | 9.2 |  |  | 8.2 |  |  | 25.2 |  |
| Confl. Peds. (\#/hr) | 5 |  | 5 | 5 |  | 5 | 5 |  | 5 | 5 |  | 5 |
| Confl. Bikes (\#/hr) |  |  | 5 |  |  | 5 |  |  | 5 |  |  | 5 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 5\% | 5\% | 5\% | 5\% | 5\% | 5\% | 5\% | 5\% | 5\% | 5\% | 5\% | 5\% |
| Adj. Flow (vph) | 23 | 1 | 288 | 13 | 1 | 5 | 484 | 520 | 30 | 2 | 425 | 42 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 0 | 24 | 288 | 0 | 19 | 0 | 484 | 550 | 0 | 2 | 467 | 0 |
| Turn Type | Perm | NA | Perm | Perm | NA |  | pm+pt | NA |  | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  | 5 | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  |  | 2 |  |  | 6 |  |  |
| Detector Phase | 4 | 4 | 4 | 8 | 8 |  | 5 | 2 |  | 6 | 6 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |  | 6.0 | 10.0 |  | 10.0 | 10.0 |  |
| Minimum Split (s) | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 |  | 12.0 | 26.0 |  | 26.0 | 26.0 |  |
| Total Split (s) | 26.0 | 26.0 | 26.0 | 26.0 | 26.0 |  | 16.0 | 64.0 |  | 48.0 | 48.0 |  |
| Total Split (\%) | 28.9\% | 28.9\% | 28.9\% | 28.9\% | 28.9\% |  | 17.8\% | 71.1\% |  | 53.3\% | 53.3\% |  |
| Maximum Green (s) | 20.0 | 20.0 | 20.0 | 20.0 | 20.0 |  | 10.0 | 58.0 |  | 42.0 | 42.0 |  |
| Yellow Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| All-Red Time (s) | 2.0 | 2.0 | 2.0 | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  |
| Lost Time Adjust (s) |  | 0.0 | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Lost Time (s) |  | 6.0 | 6.0 |  | 6.0 |  | 6.0 | 6.0 |  | 6.0 | 6.0 |  |
| Lead/Lag |  |  |  |  |  |  | Lead |  |  | Lag | Lag |  |
| Lead-Lag Optimize? |  |  |  |  |  |  | Yes |  |  | Yes | Yes |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Recall Mode | None | None | None | None | None |  | Max | Max |  | Max | Max |  |
| Walk Time (s) | 8.0 | 8.0 | 8.0 | 8.0 | 8.0 |  |  | 8.0 |  | 8.0 | 8.0 |  |
| Flash Dont Walk (s) | 12.0 | 12.0 | 12.0 | 12.0 | 12.0 |  |  | 12.0 |  | 12.0 | 12.0 |  |
| Pedestrian Calls (\#/hr) | 5 | 5 | 5 | 5 | 5 |  |  | 5 |  | 5 | 5 |  |
| Act Effct Green (s) |  | 11.8 | 11.8 |  | 11.8 |  | 58.1 | 58.1 |  | 42.1 | 42.1 |  |


| $\rangle$ |  |  |  |  |  | 4 | $\dagger$ |  |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Actuated g/C Ratio | 0.14 | 0.14 |  | 0.14 |  | 0.71 | 0.71 |  | 0.51 | 0.51 |  |
| v/c Ratio | 0.13 | 0.63 |  | 0.09 |  | 0.84 | 0.44 |  | 0.00 | 0.51 |  |
| Control Delay | 31.5 | 10.8 |  | 25.4 |  | 22.6 | 6.8 |  | 11.5 | 16.2 |  |
| Queue Delay | 0.0 | 0.0 |  | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 |  |
| Total Delay | 31.5 | 10.8 |  | 25.4 |  | 22.6 | 6.8 |  | 11.5 | 16.2 |  |
| LOS | C | B |  | C |  | C | A |  | B | B |  |
| Approach Delay | 12.4 |  |  | 25.4 |  |  | 14.2 |  |  | 16.1 |  |
| Approach LOS | B |  |  | C |  |  | B |  |  | B |  |
| Queue Length 50th ( m ) | 3.1 | 0.0 |  | 1.8 |  | 21.1 | 24.4 |  | 0.1 | 38.9 |  |
| Queue Length 95th (m) | 8.9 | 18.2 |  | 6.9 |  | \#79.2 | 60.0 |  | 1.3 | 77.7 |  |
| Internal Link Dist (m) | 130.6 |  |  | 103.5 |  |  | 112.8 |  |  | 395.6 |  |
| Turn Bay Length ( m ) |  | 15.0 |  |  |  | 90.0 |  |  | 15.0 |  |  |
| Base Capacity (vph) | 319 | 574 |  | 341 |  | 576 | 1258 |  | 418 | 907 |  |
| Starvation Cap Reductn | 0 | 0 |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 |  | 0 |  | 0 | 0 |  | 0 | 0 |  |
| Reduced v/c Ratio | 0.08 | 0.50 |  | 0.06 |  | 0.84 | 0.44 |  | 0.00 | 0.51 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 90 |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 82 |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 80 |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Semi Act-Uncoord |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.84 |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 14.5 |  |  |  | Intersection LOS: B |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 72.3\% |  |  |  | ICU Level of Service C |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 6: Tk 2 \& Wickwire North/Robert Scott


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 6.8 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | T | $\mathbf{7}$ |  | 4 | $\mathbf{b}$ |  |
| Traffic Vol, veh/h | 104 | 265 | 117 | 237 | 235 | 70 |
| Future Vol, veh/h | 104 | 265 | 117 | 237 | 235 | 70 |
| Conflicting Peds, \#/hr | 5 | 5 | 5 | 0 | 0 | 5 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 15 | 15 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 5 | 5 | 5 | 5 | 5 | 5 |
| Mvmt Flow | 113 | 288 | 127 | 258 | 255 | 76 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 6.7 |  |  |  |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | 7 | $\mathbf{r}$ |  | 4 | $\mathbf{b}$ |  |
| Traffic Vol, veh/h | 74 | 151 | 230 | 274 | 281 | 95 |
| Future Vol, veh/h | 74 | 151 | 230 | 274 | 281 | 95 |
| Conflicting Peds, \#/hr | 5 | 5 | 5 | 0 | 0 | 5 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | 15 | 15 | - | - | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 92 | 92 | 92 | 92 | 92 | 92 |
| Heavy Vehicles, \% | 5 | 5 | 5 | 5 | 5 | 5 |
| Mvmt Flow | 80 | 164 | 250 | 298 | 305 | 103 |




[^0]:    East Milford Mixed Use Development

[^1]:    East Milford Mixed Use Development
    Page |iii Traffic Impact Study

[^2]:    A - Queue represents the calculated vehicle queue length in metres occurring 95\% of the time (95 ${ }^{\text {th }}$ percentile).
    $B$ - HCM methodology assumes no delay for this first order intersection movement. No results calculated.

[^3]:    ${ }^{1}$ It should be noted that the proposed East Milford Mixed Use development will form the north limit of the MEH's Regional Service Boundary (RSB) area.

[^4]:    ${ }^{2}$ The 2021 forecast volumes included traffic associated with 400 new residential units built between 2017 and 2021.

[^5]:    A - Intersection does not exist under this development scenario.
    $B$ - Assumes the existing three-leg intersection is converted to a four-leg intersection to accommodate the new west access connection serving the Wickwire Development.

[^6]:    A - Queue represents the calculated vehicle queue length in metres occurring 95\% of the time (95 ${ }^{\text {th }}$ percentile).
    $B-H C M$ methodology assumes no delay for this first order intersection movement. No results calculated.
    $C$ - Intersection does not exist under this scenario.

[^7]:    ${ }^{3}$ Geometric Design Guide for Canadian Roads. Transportation Association of Canada. 2017 Edition.

